



FAES - L2

Solar collectors

- types
- efficiency
- application
- statistics



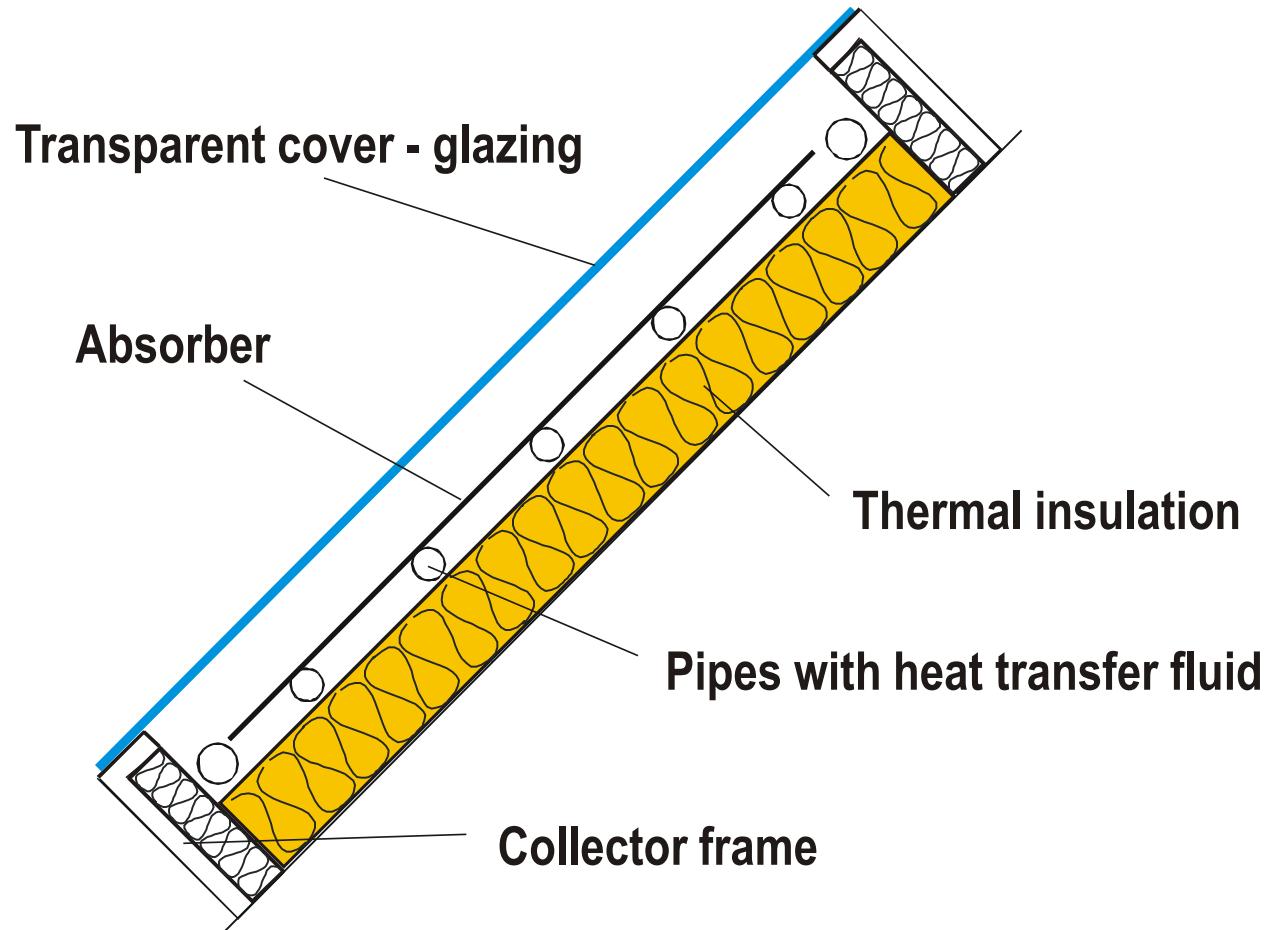


Photothermal conversion

- **collecting surface (collector)**
surface absorbing solar radiation which converts to heat
- **accumulation (heat storage)**
storing the solar heat gains for further use
(storage tank, wall, mass in the building space, ...)
- **consumer**
hot water, heating, cooling, ...

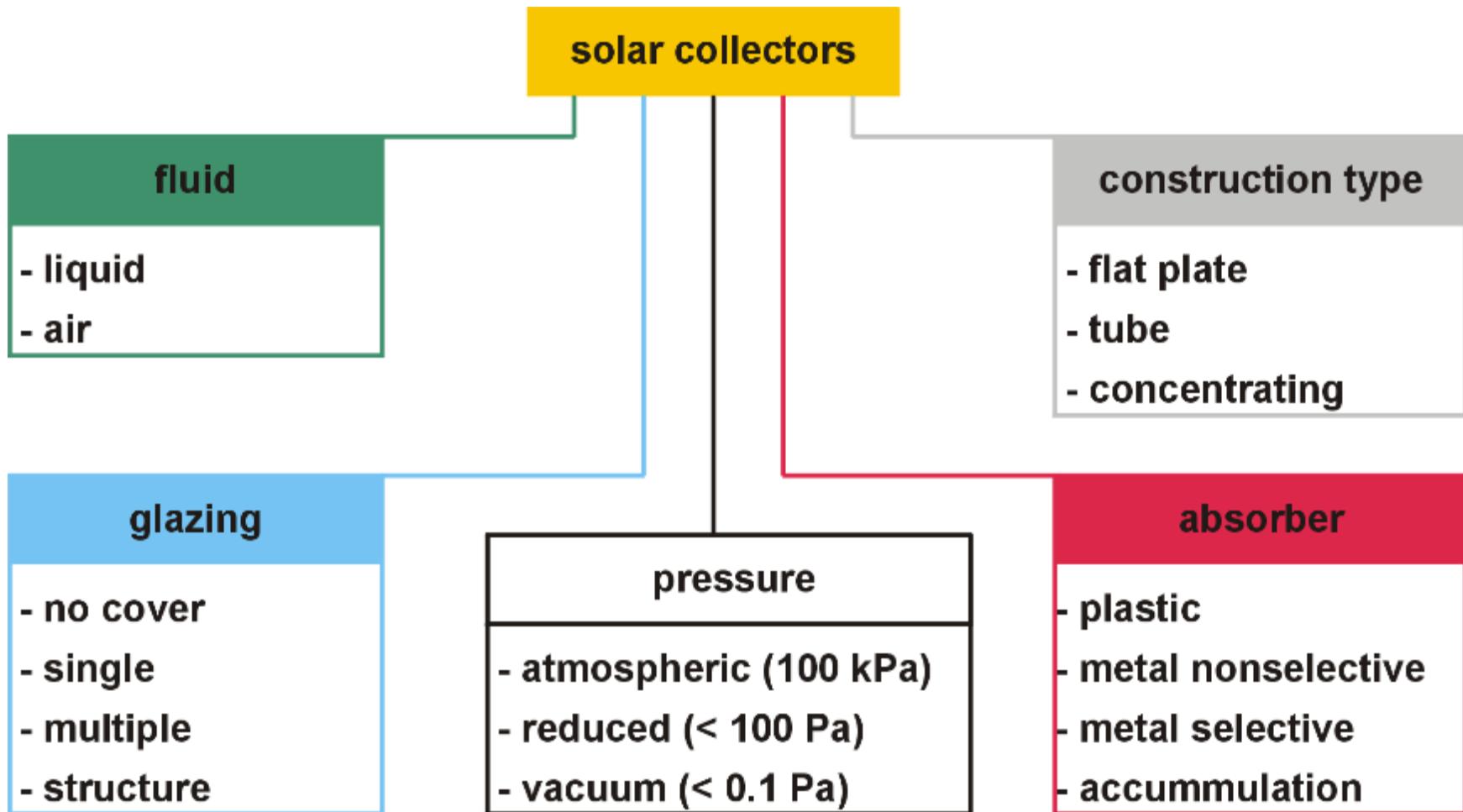


Solar collector



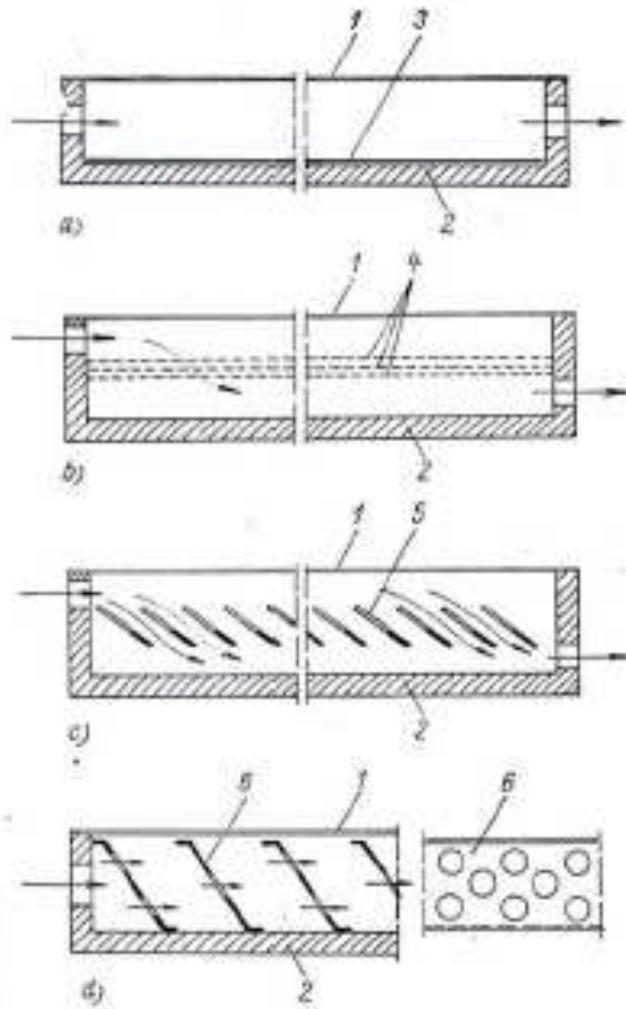


Solar collectors





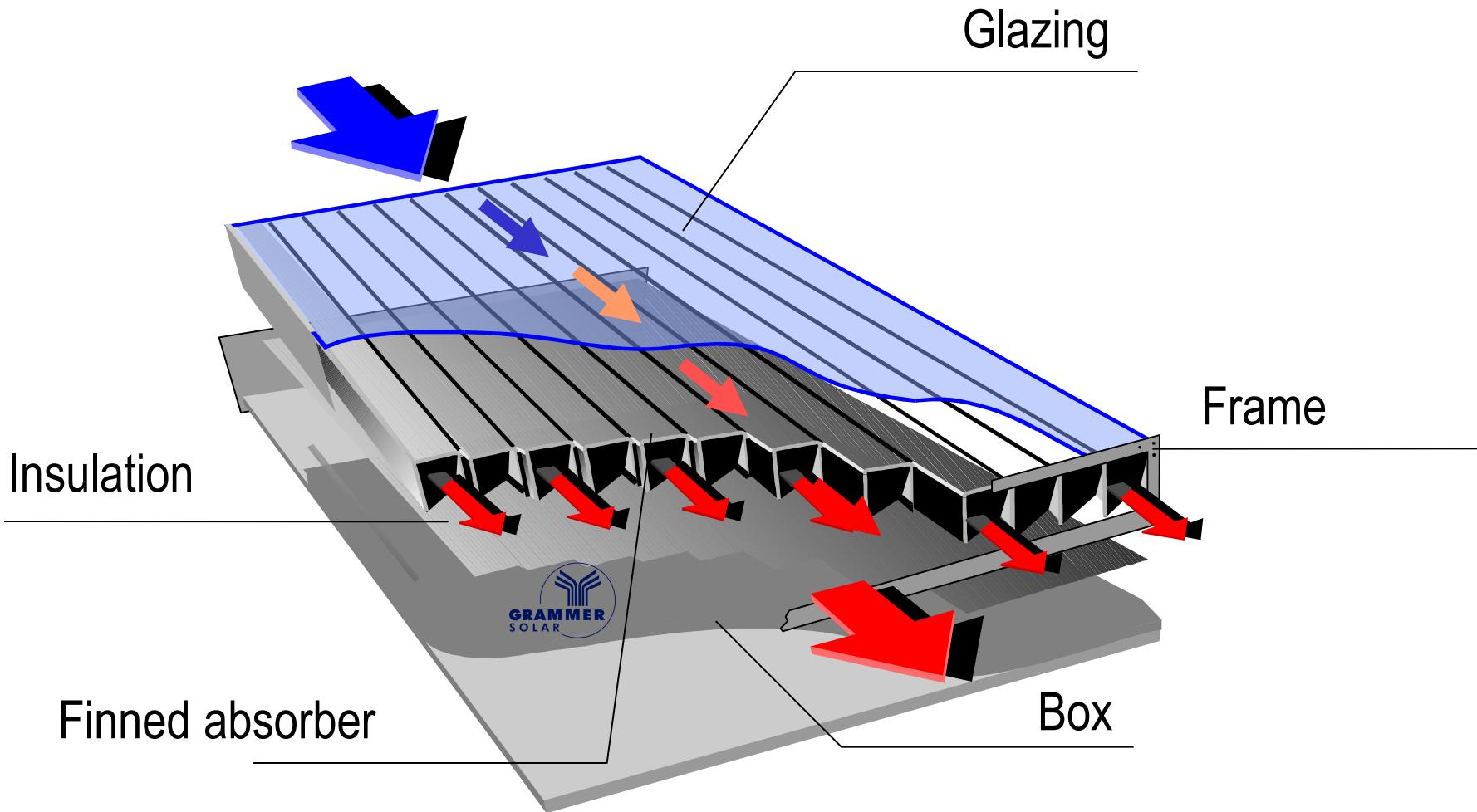
Solar air collectors



- heat transfer fluid is **air**
- heats from outer surface of absorber
- low heat capacity, high flowrates, large dimensions
- high auxiliary electricity use
- **applications:**
 - agriculture – drying
 - residential – heating of ventilation air

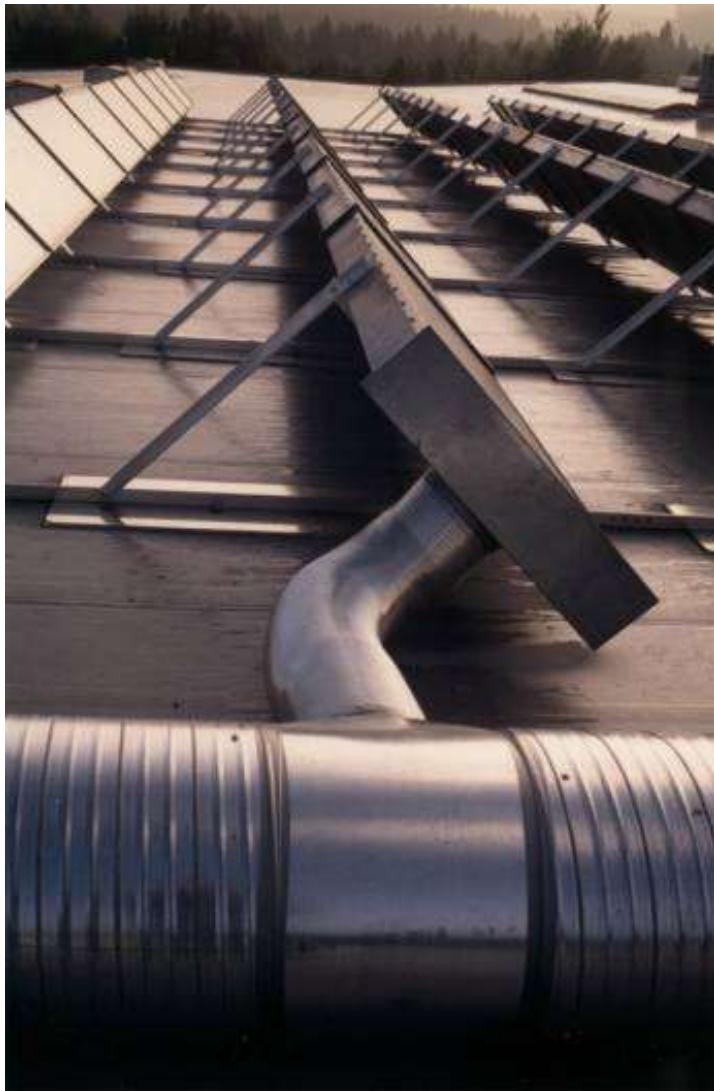


Solar air collectors



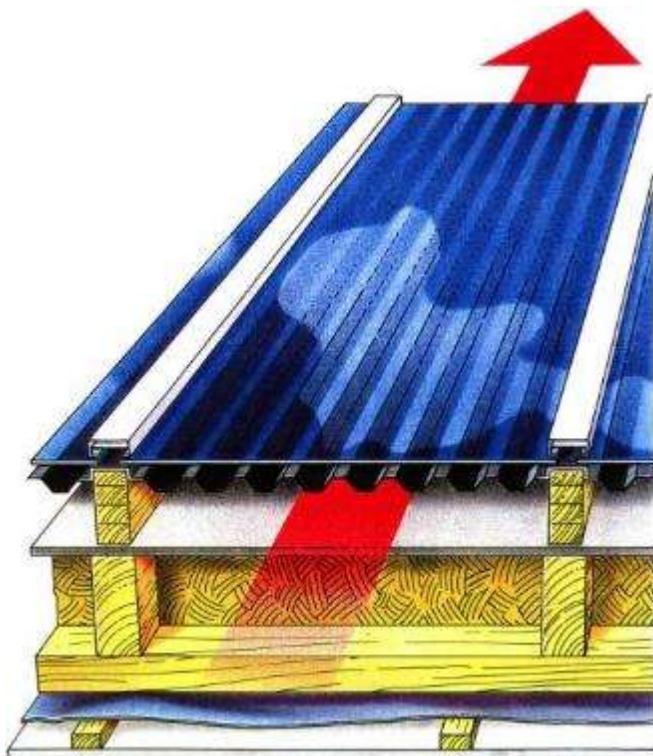


Solar air collectors





Solar air collectors



integration into roof



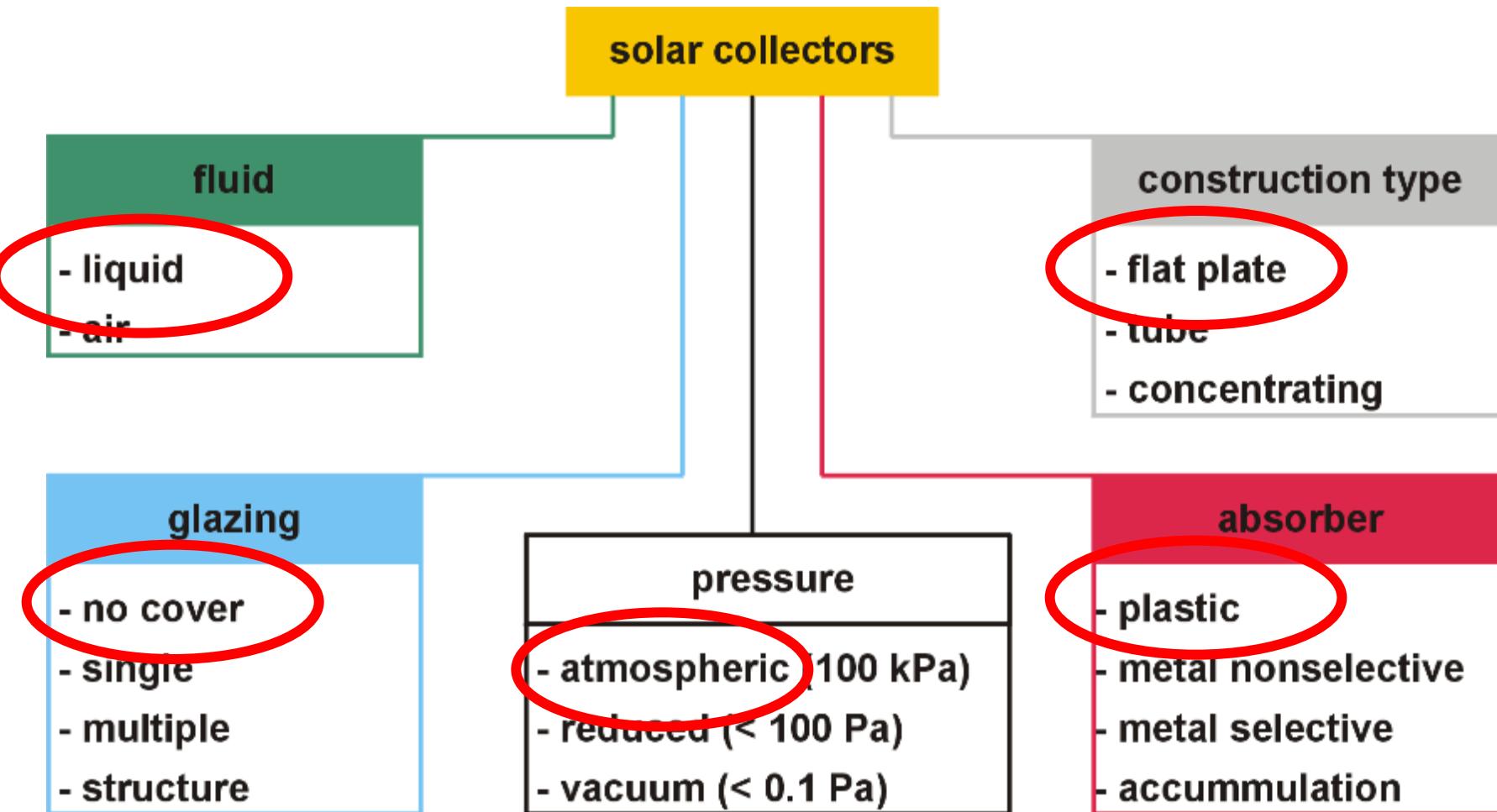
Solar liquid collectors

- liquid as heat transfer fluid
(water, antifreeze, oil, etc.)
- energy absorbed at surface is removed by heat transfer liquid flowing inside pipes of absorber





Solar collectors





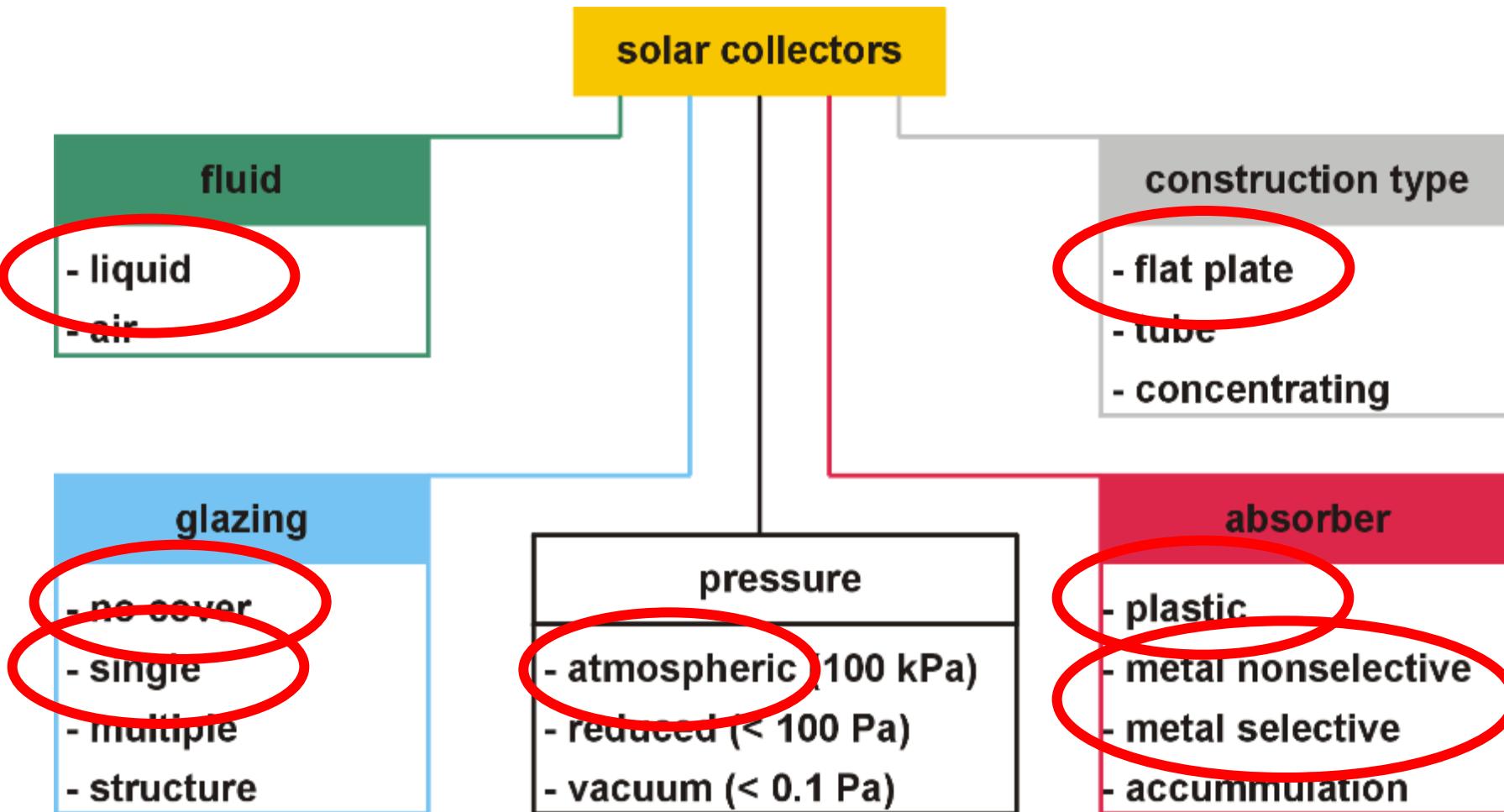
Unglazed solar collectors

- temperature level < 40 °C
- seasonal applications, swimming pools
- strongly dependent on ambient conditions (temperature, wind)





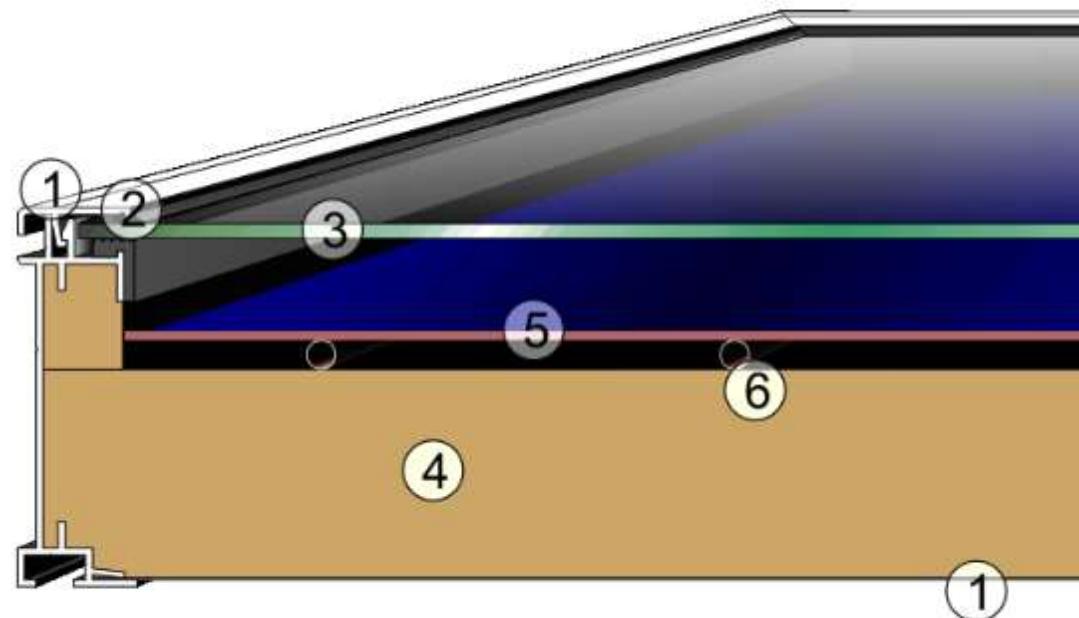
Solar collectors





Flat plate covered solar collectors

- 1 frame
- 2 sealing
- 3 transparent cover
- 4 thermal insulation
- 5 absorber
- 6 pipe register





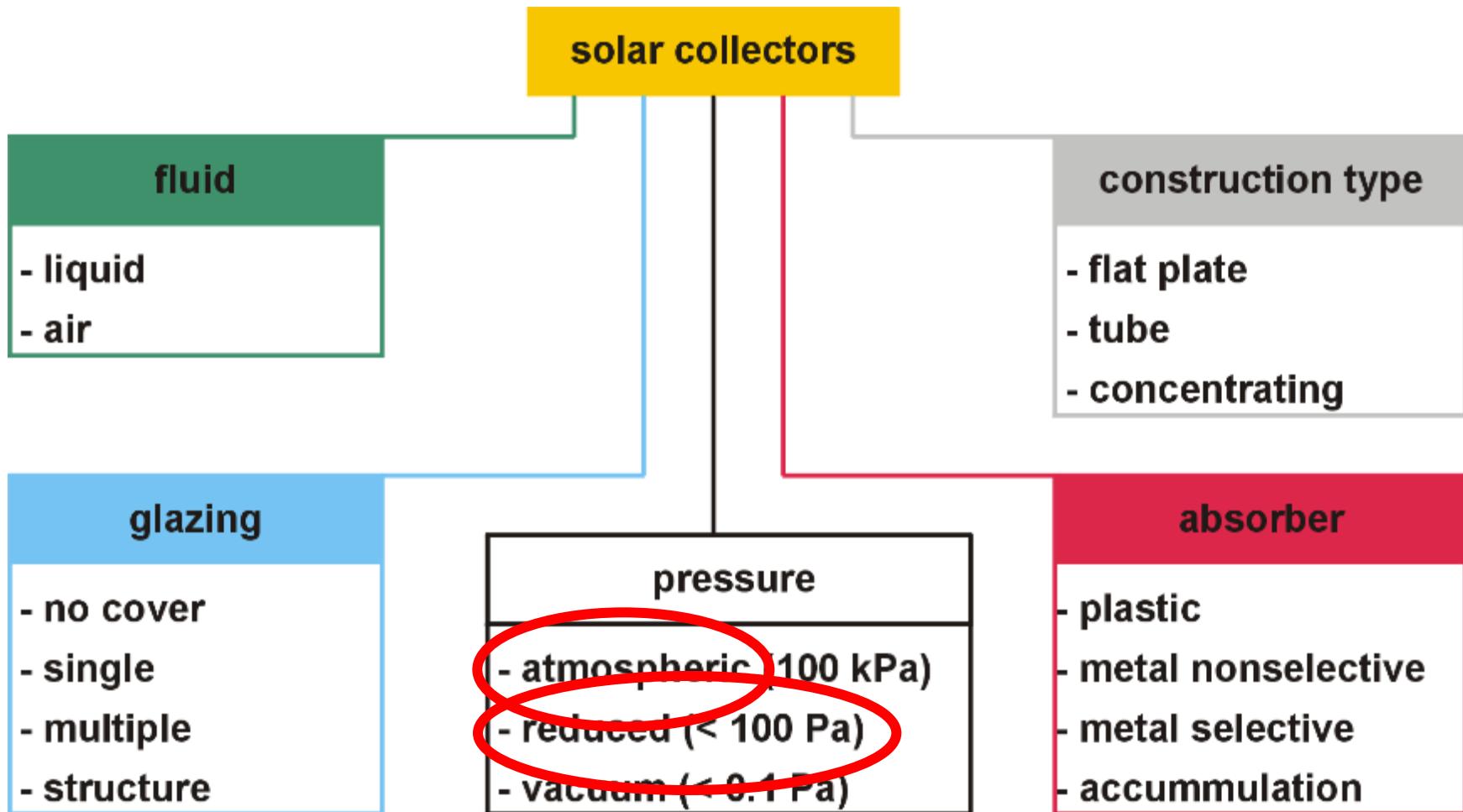
Flat plate solar collectors

- suitable for building envelope integration
 - roof
 - facade





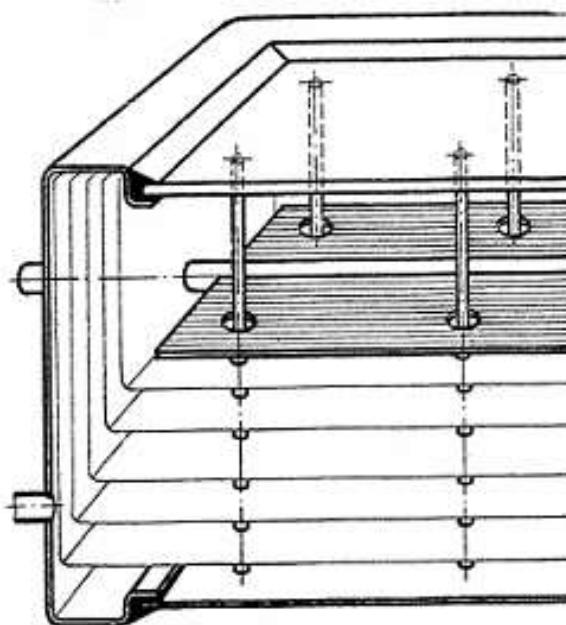
Solar collectors





Vacuum flat plate solar collectors

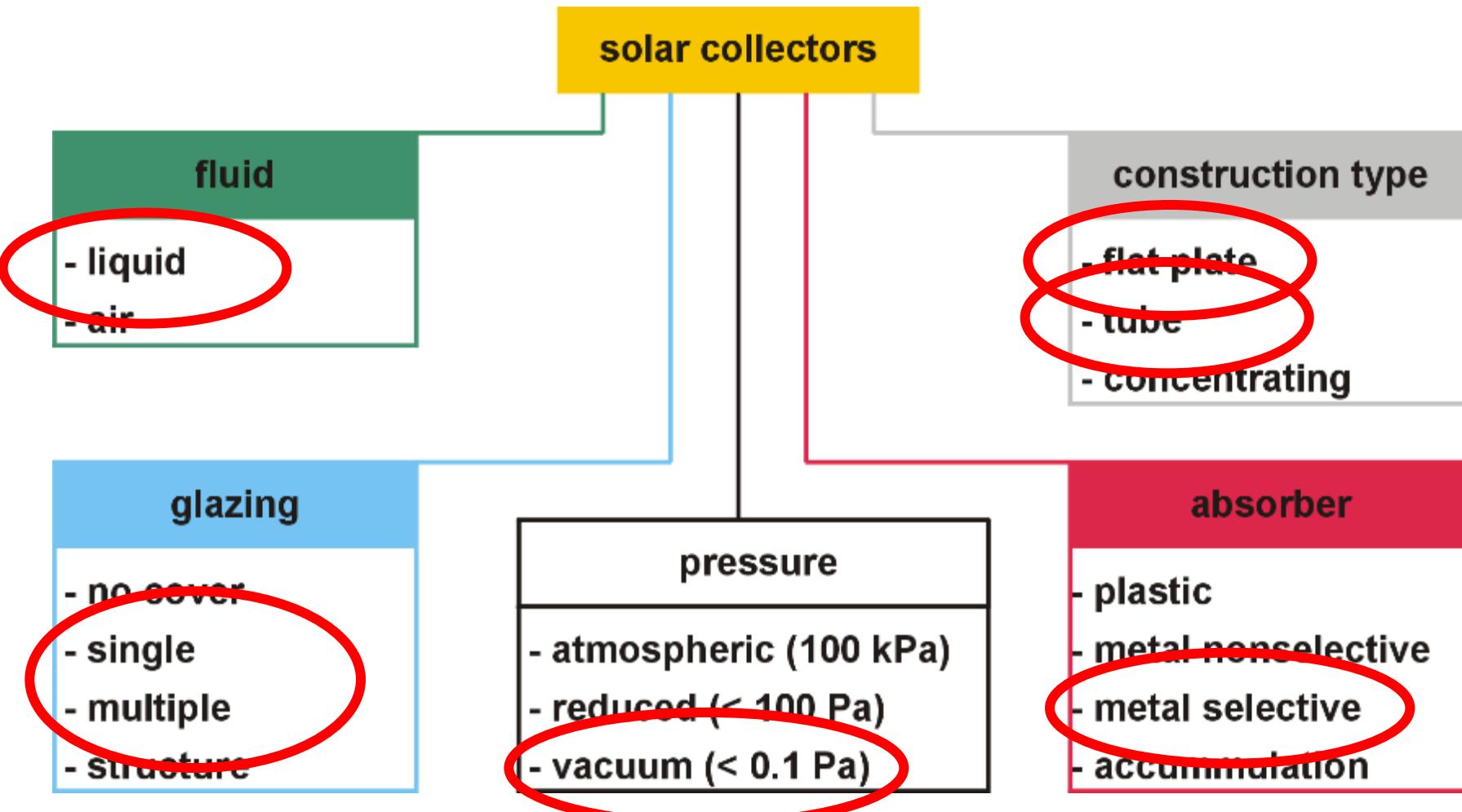
underpressure to reduce heat loss (absolute pressure **1 to 10 kPa**)
load upon flat cover glazing (pillars)



need for shading the radiation heat transfer
to back side (IR reflectors)



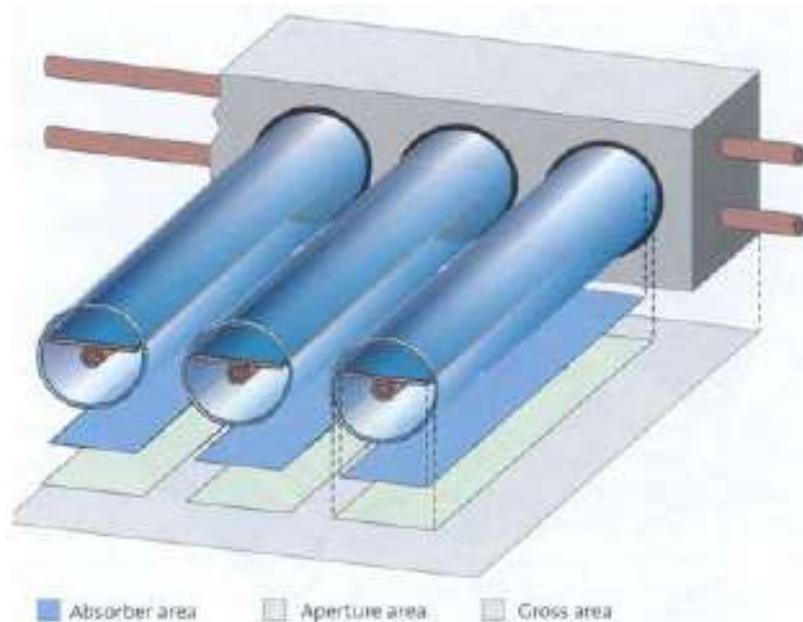
Solar collectors





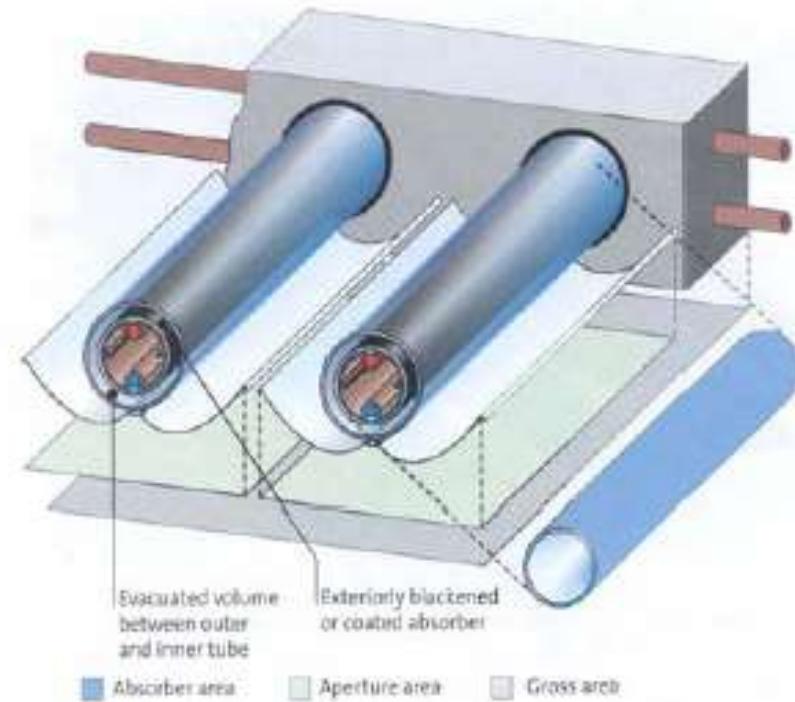
Vacuum tube solar collectors

single vacuum tube
flat absorber



high vacuum 1 mPa

**double vacuum tube (Sydney)
cylindric absorber**

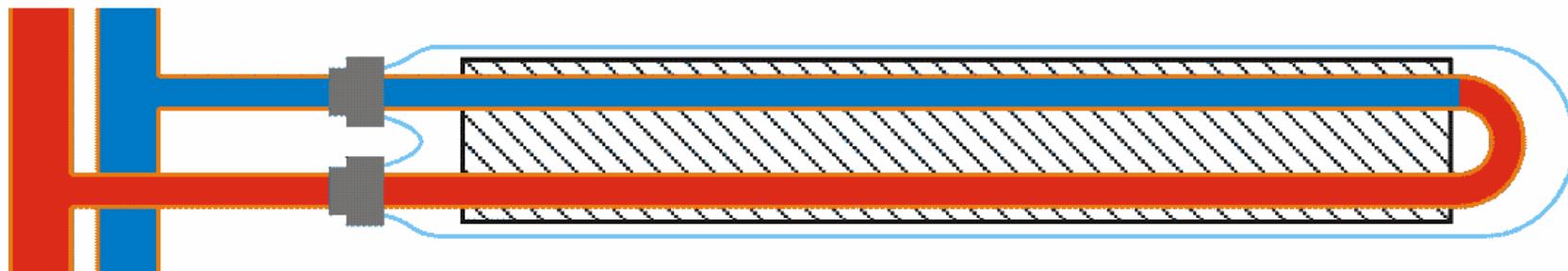
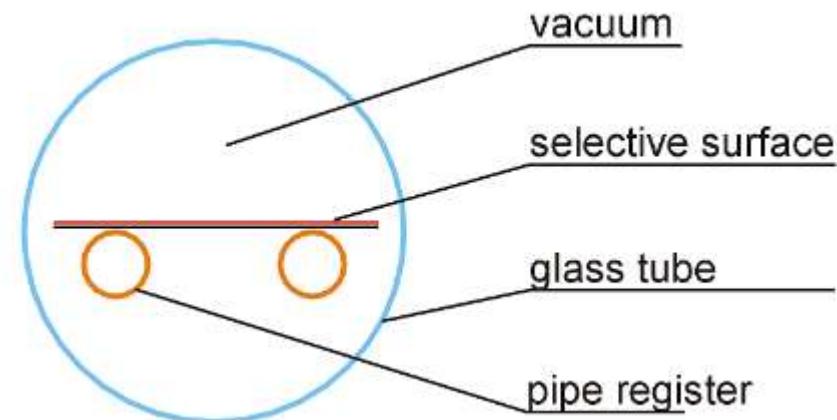




Vacuum tube solar collectors single vacuum tube

Single vacuum tube with flat absorber

- direct flow (DF)



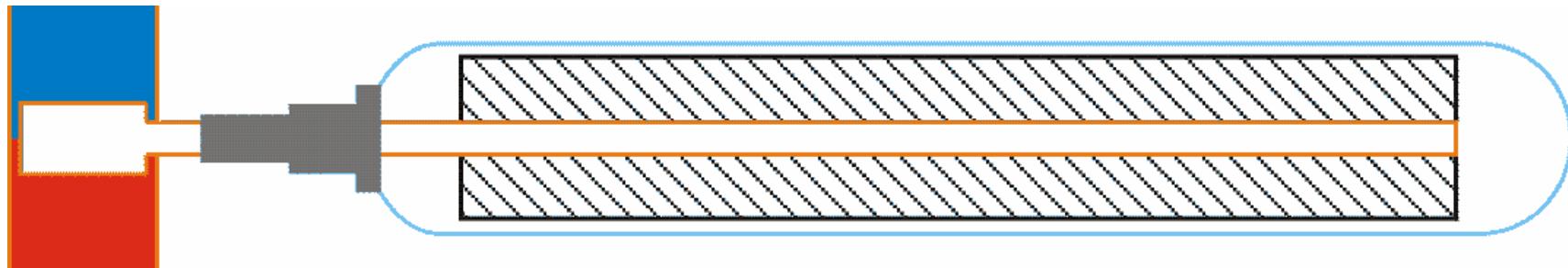
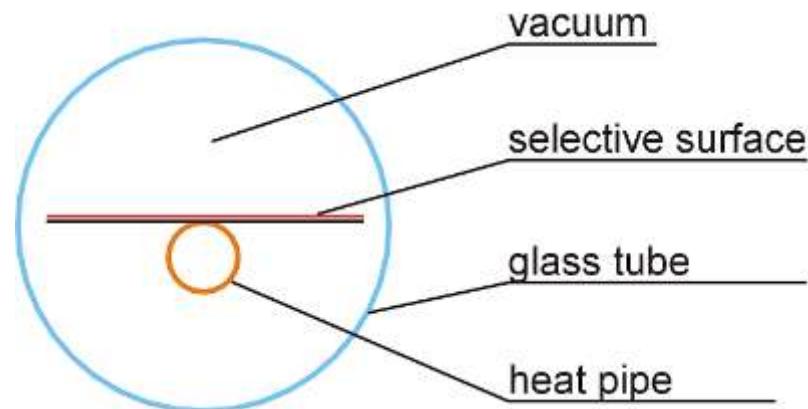
high quality heat transfer from absorber into fluid



Vacuum tube solar collectors single vacuum tube

Single vacuum tube with flat absorber

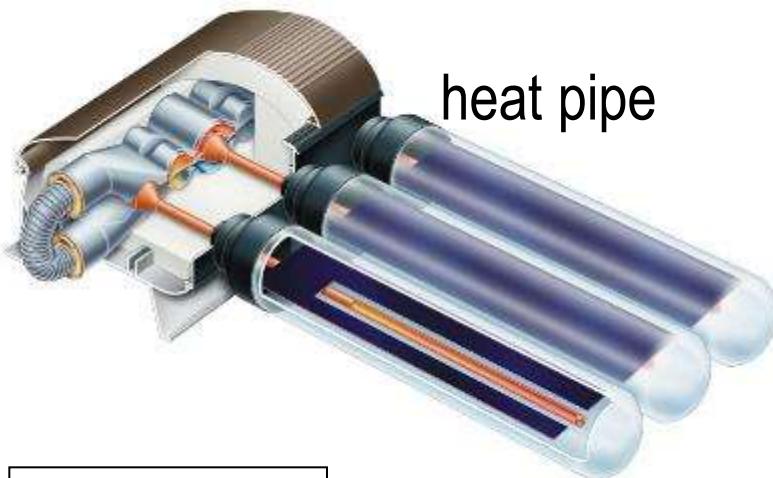
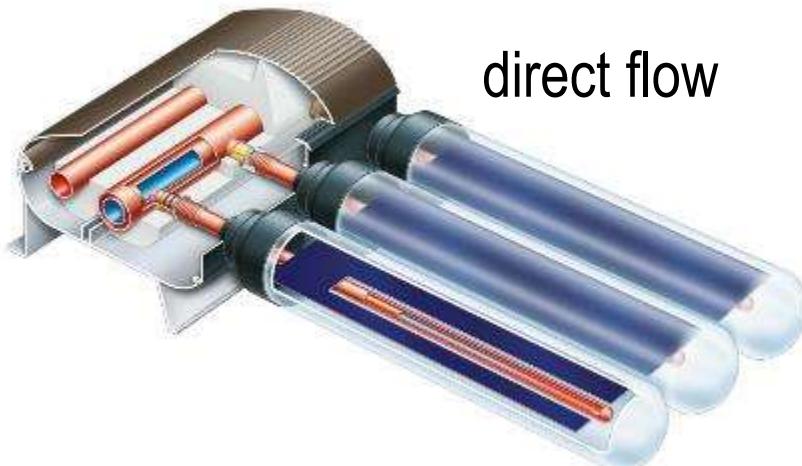
- heat pipe (HP)



high quality heat transfer from absorber to evaporator part



Vacuum tube solar collectors single vacuum tube

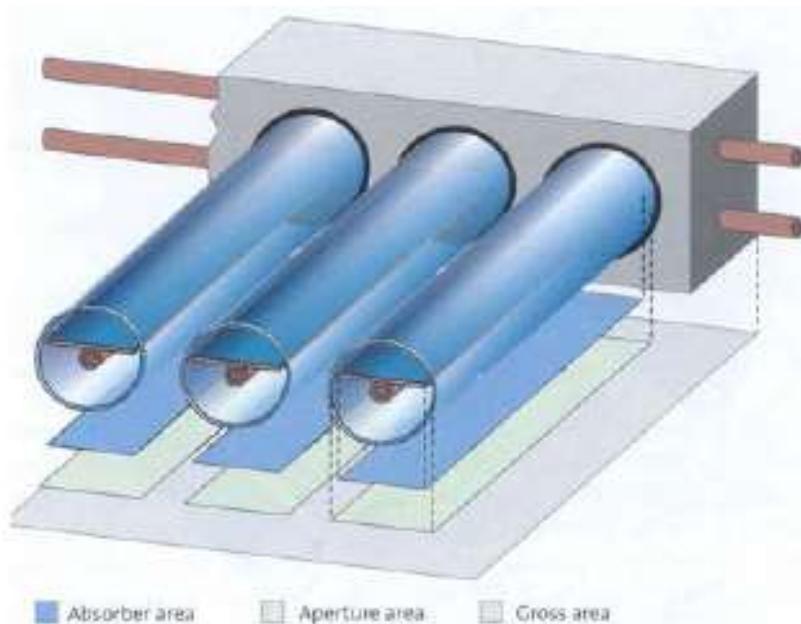


source: Viessmann

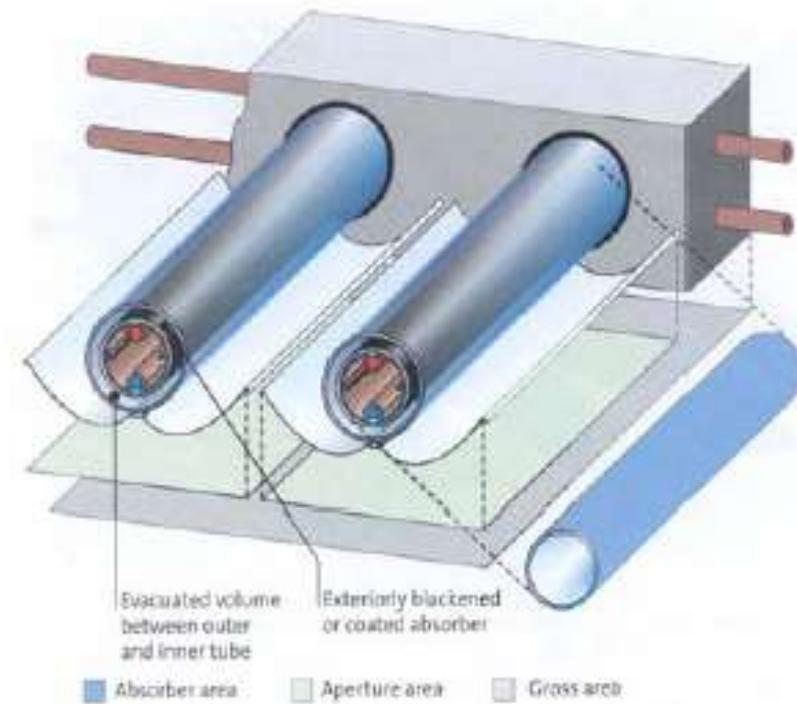


Vacuum tube solar collectors

**single vacuum tube
flat absorber**



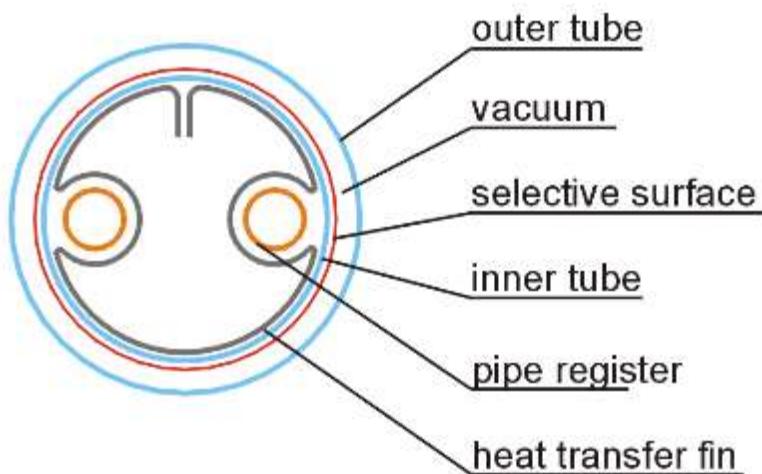
**double vacuum tube (Sydney)
cylindric absorber**



high vacuum 1 mPa

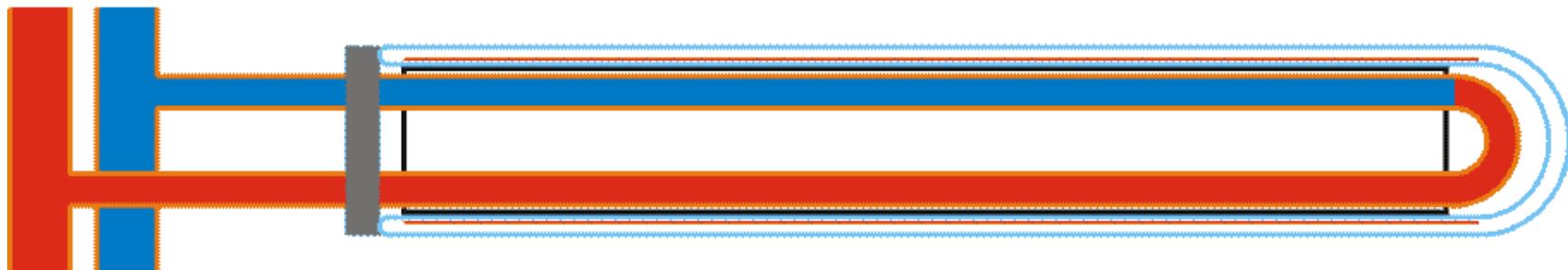


Vacuum tube solar collectors double vacuum tube



Double vacuum Sydney tube with cylindric absorber

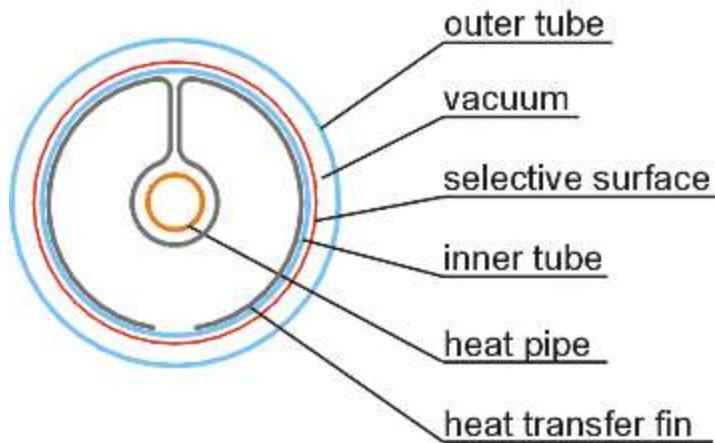
- direct flow (DF)
with a contact fin



heat transfer fin between absorber tube and pipe register needed!

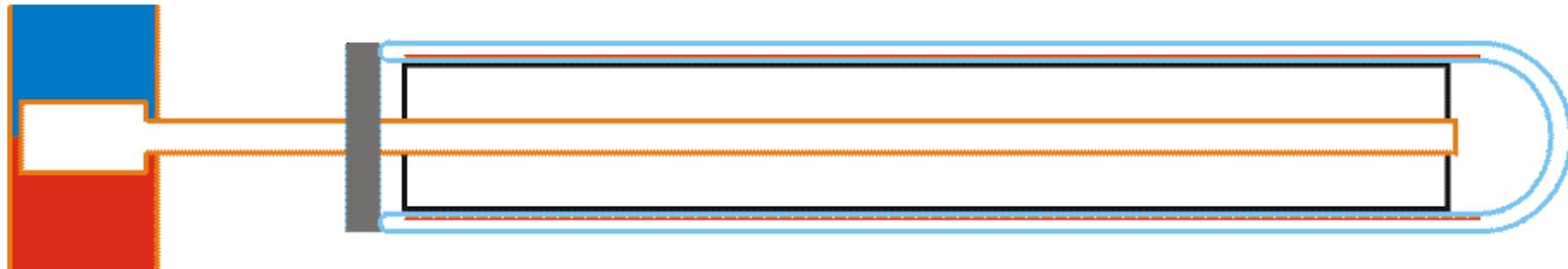


Vacuum tube solar collectors double vacuum tube



Double vacuum Sydney tube with cylindric absorber

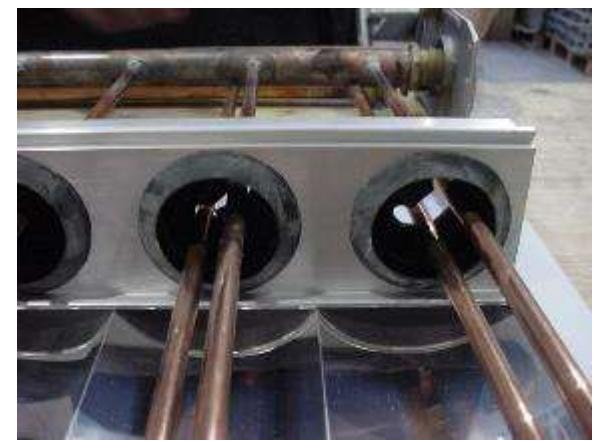
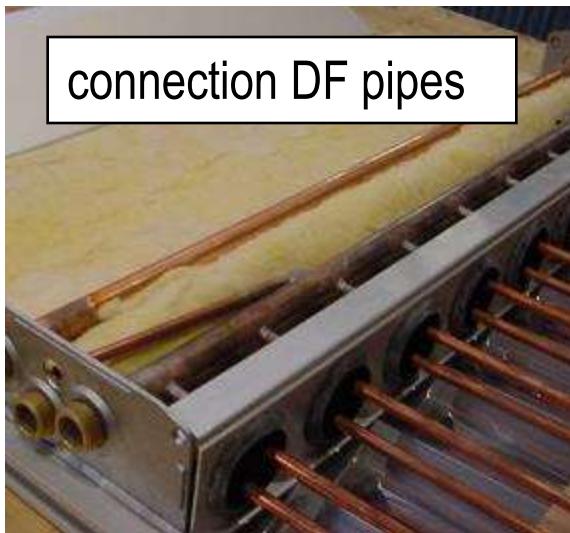
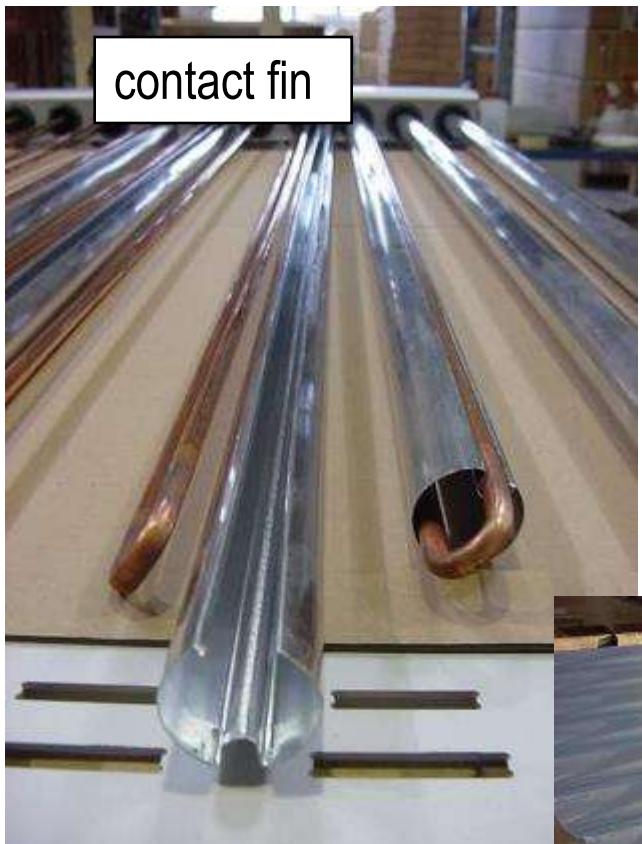
- heat pipe (HP)
with a contact fin



heat transfer fin between absorber tube and evaporator needed!



Vacuum tube (Sydney) solar collectors



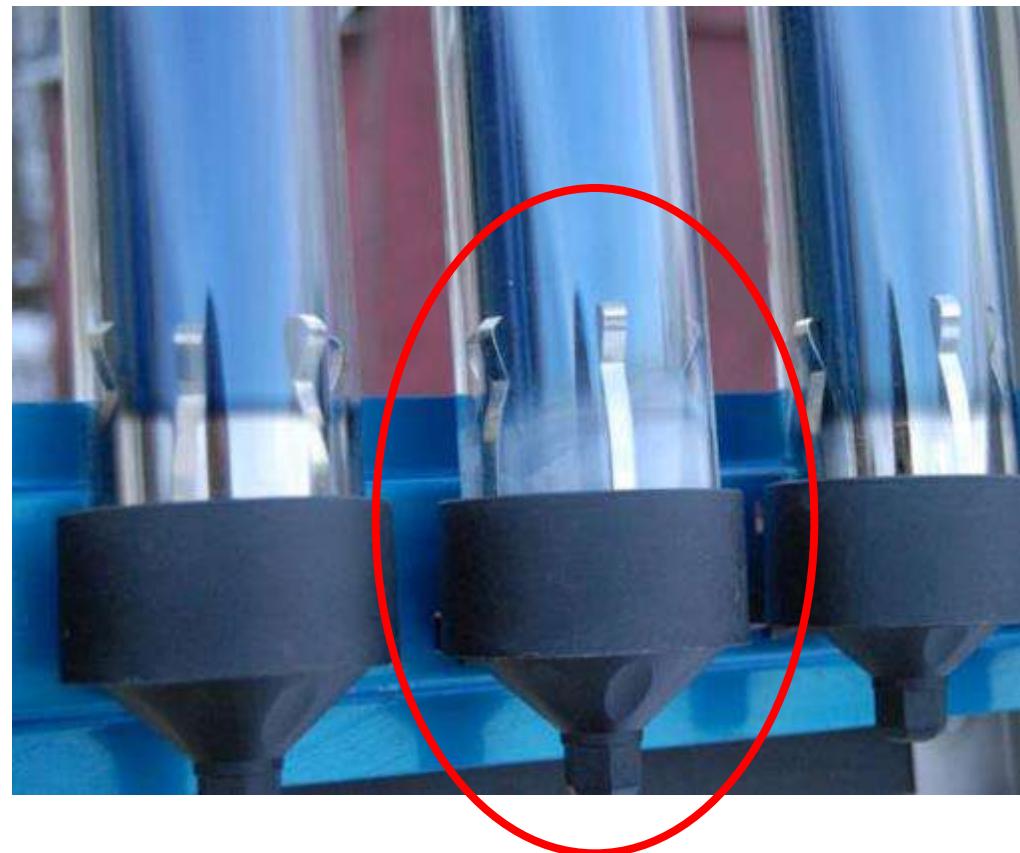
source: OPC

Vacuum tube (Sydney) solar collectors





Vacuum tube solar collectors



barium absorbs gases and
changes colour



Vacuum tube solar collectors

The getter material is held inactive in a reservoir during assembly, then heated and evaporated after initial evacuation. The vaporized getter, usually a volatile metal, instantly reacts with any residual gas, then condenses on the cool walls of the tube in a thin coating, the **getter mirror**, which continues to absorb gas.





Vacuum tube solar collectors



vacuum insulation = snow or frost removed very slowly

snow accumulation: problematic use of reflectors



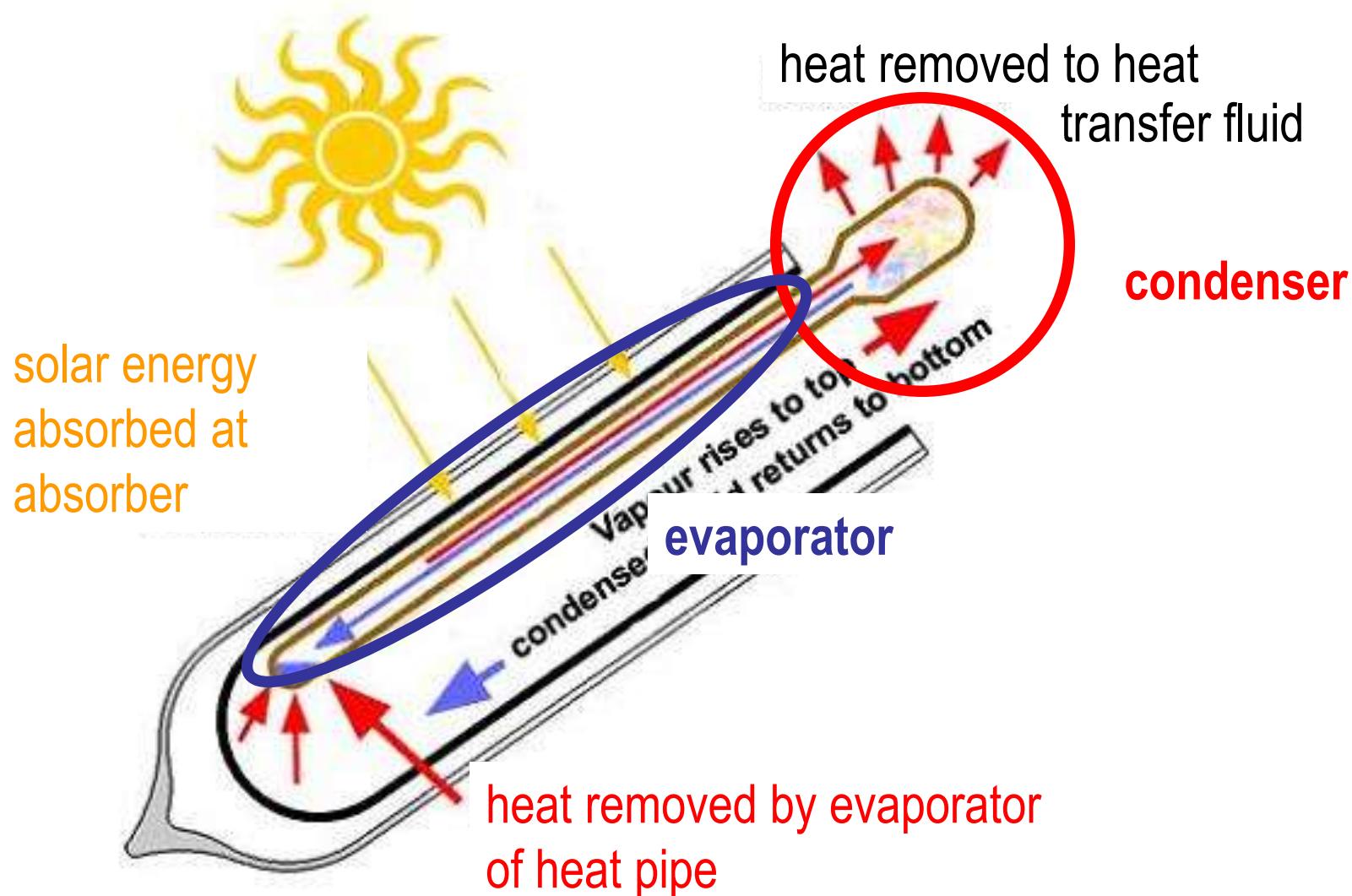
Flat plate collectors and defrosting

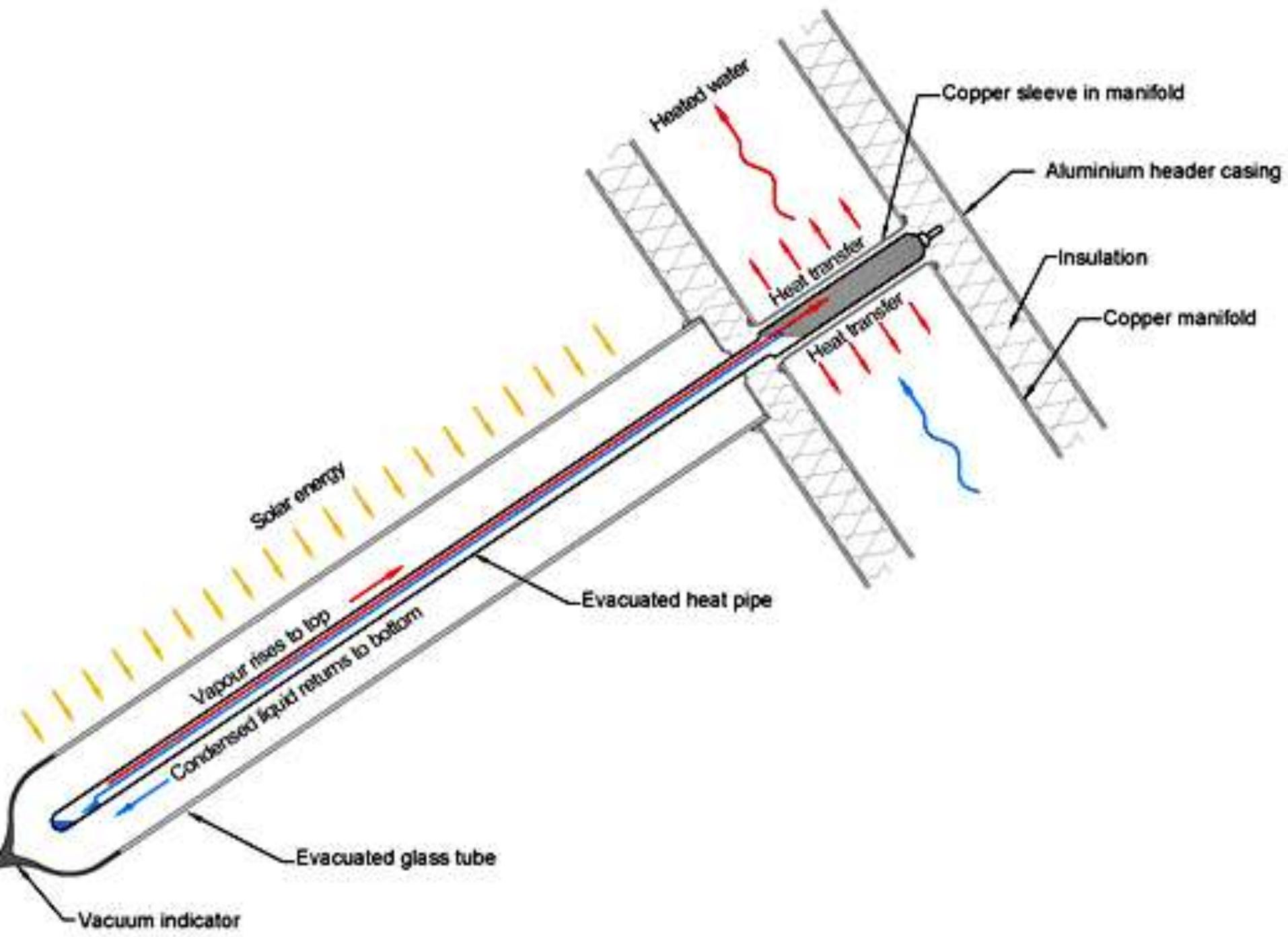


heat loss allows collector operation even in periods of snow cover



Tube collector with a heat pipe





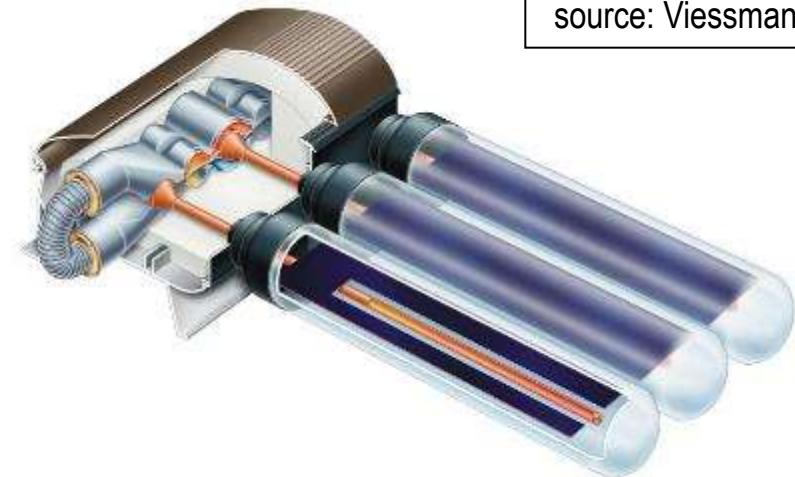


Tube collector with a heat pipe

dry connection

condenser placed in a slot

slot washed by heat transfer fluid



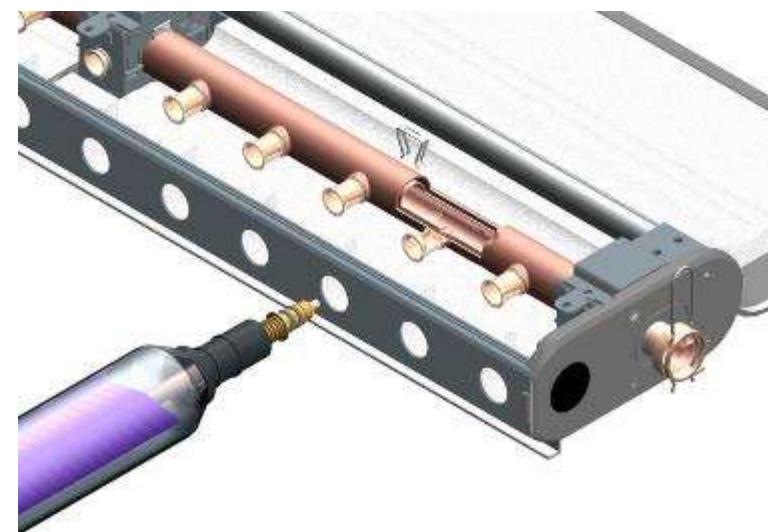


Tube collector with a heat pipe



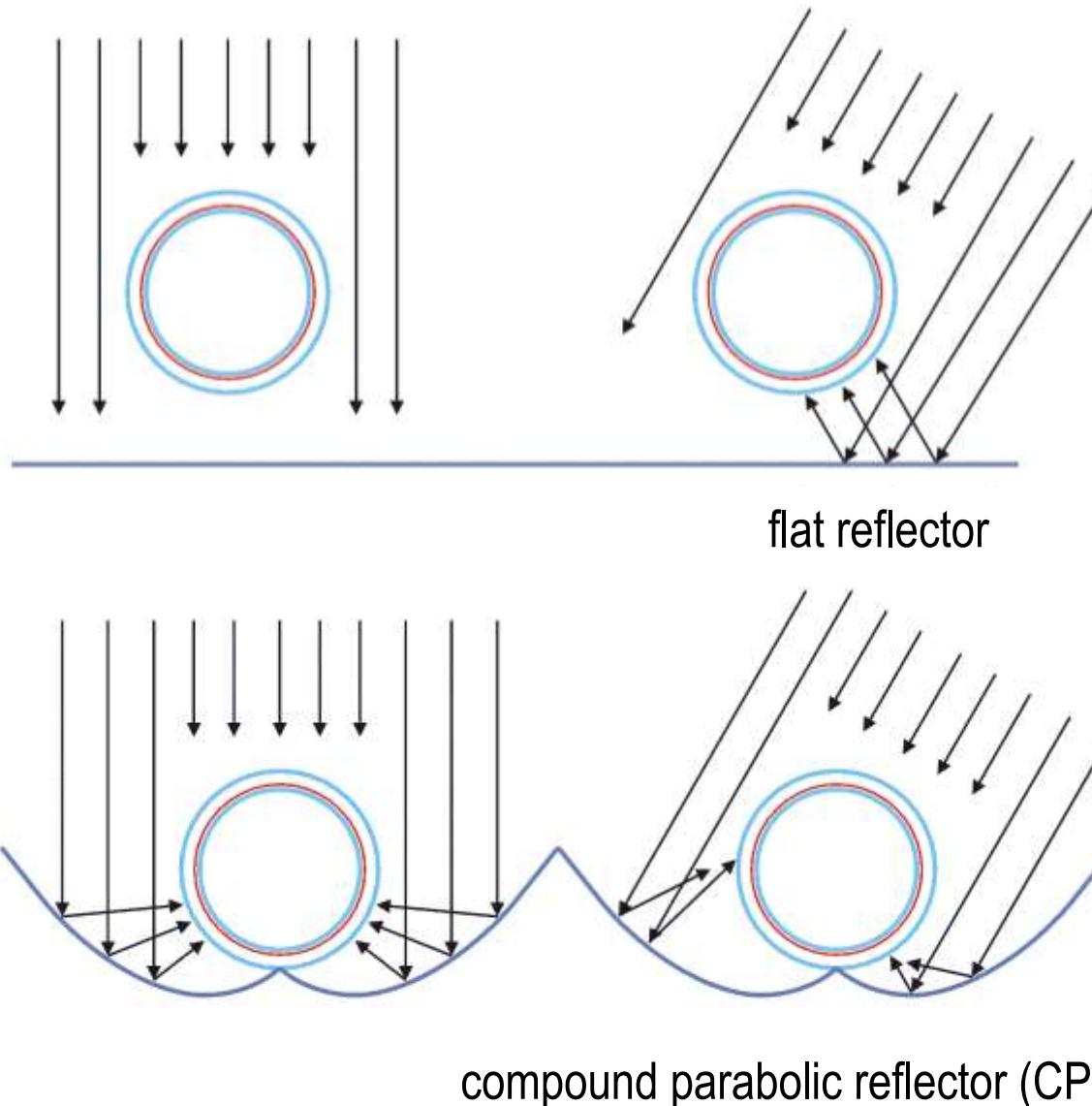
wet connection

condenser of heat pipe directly
washed by heat transfer fluid





Tube collector with a reflector



specular reflection

diffuse reflection

durability of optical
quality of reflector

snow and ice
accumulation, tube
destruction

**increase of
collector active
area (aperture)**



Concentrating solar collectors

concentration of direct solar radiation

reflection (mirrors) x refraction (lenses)

linear focus

- parabolic reflector
- Winston collector (trough form)
- collector with a Fresnel lens

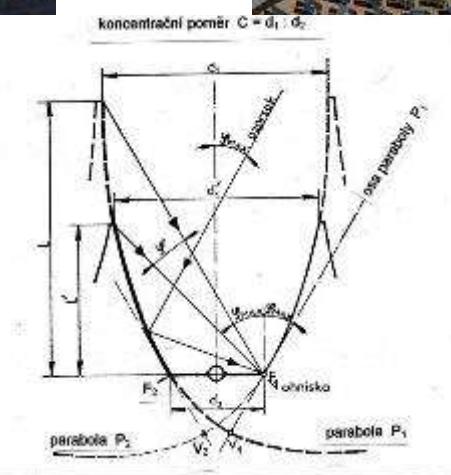
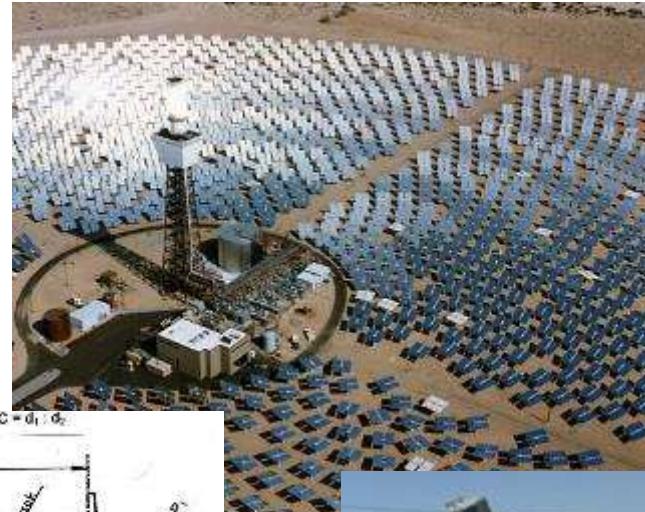
point focus

- paraboloid reflector
- heliostats



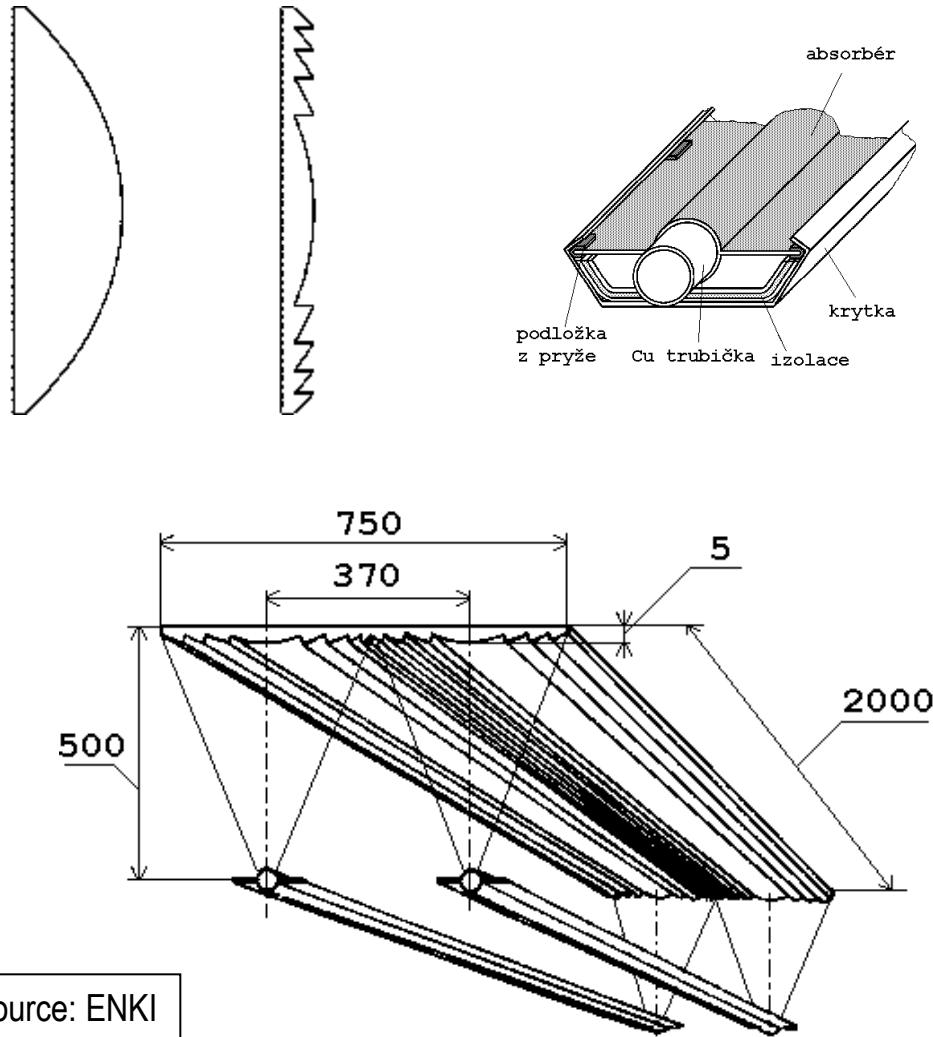


Concentrating solar collectors (reflection)





Collector with Fresnel lenses (refraction)

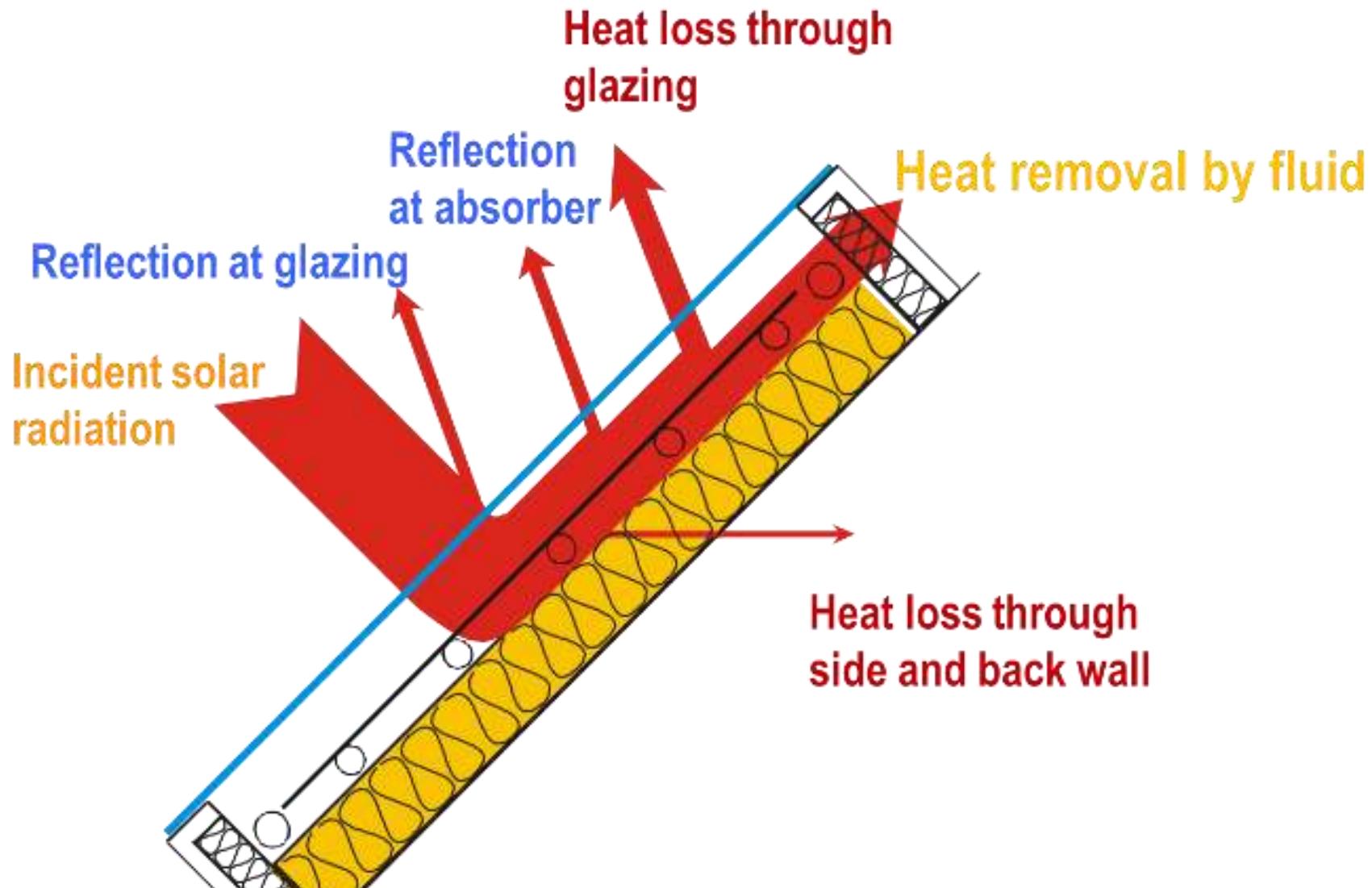


- combined active and passive component



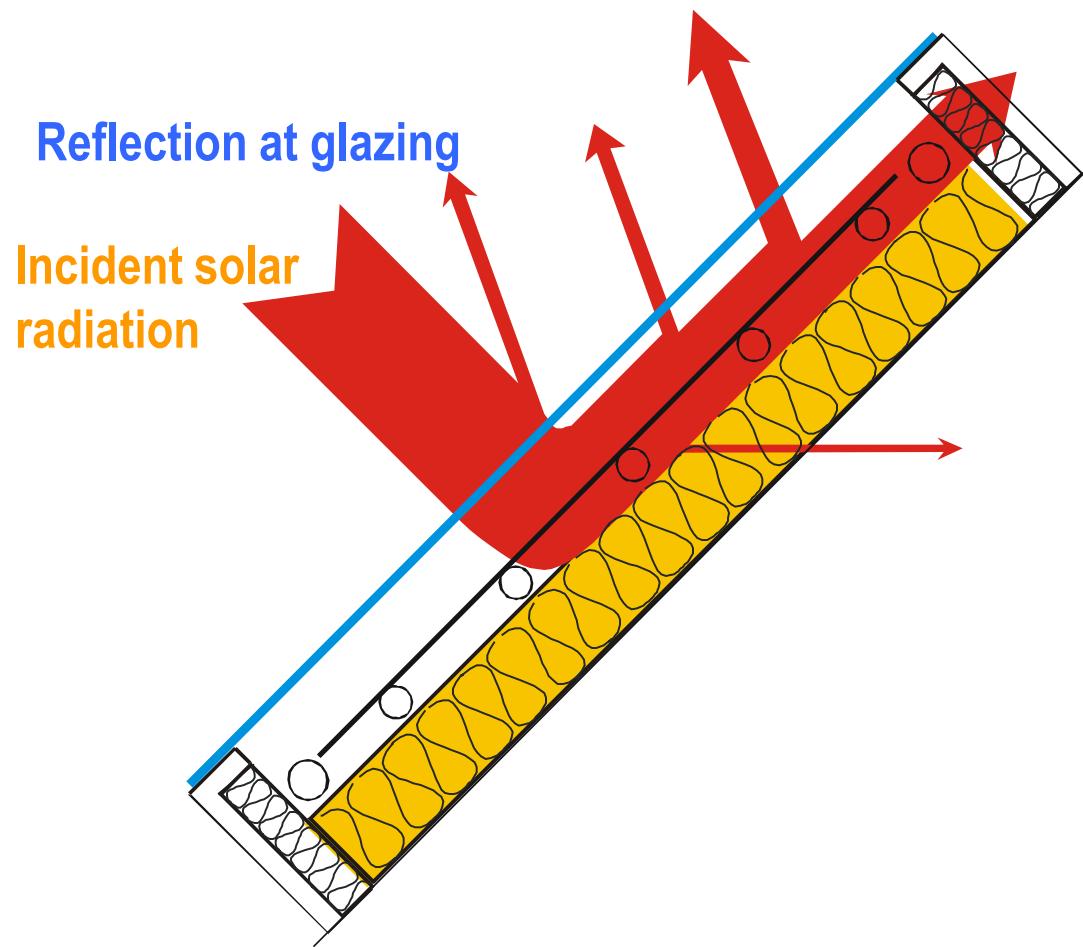


Principle and balance of solar collector





Principle and balance of solar collector





Solar collector glazing

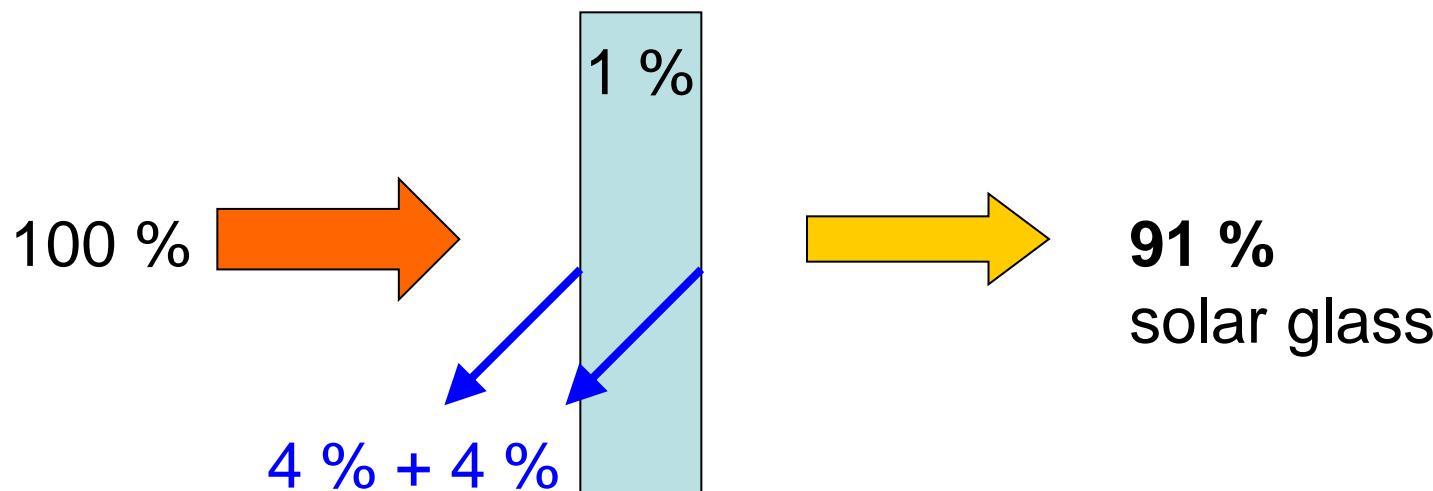
- **single glazing**
- low-iron glass, solar glass
 - low absorbance of solar radiation
- antireflective coatings
 - reduction of reflection at interface glass-air
- prismatic glass (pyramidal texture)
 - increase of transmittance at high angles





Reflection loss

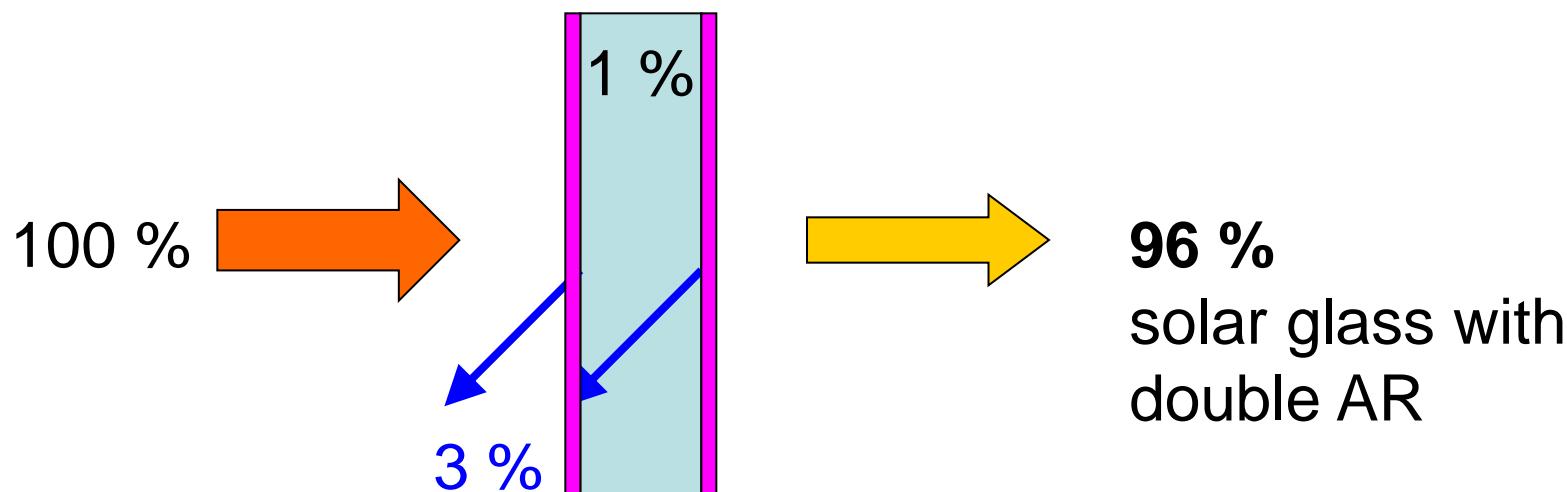
reflection at each interface glass-air 4 % (normal)
independent on thickness





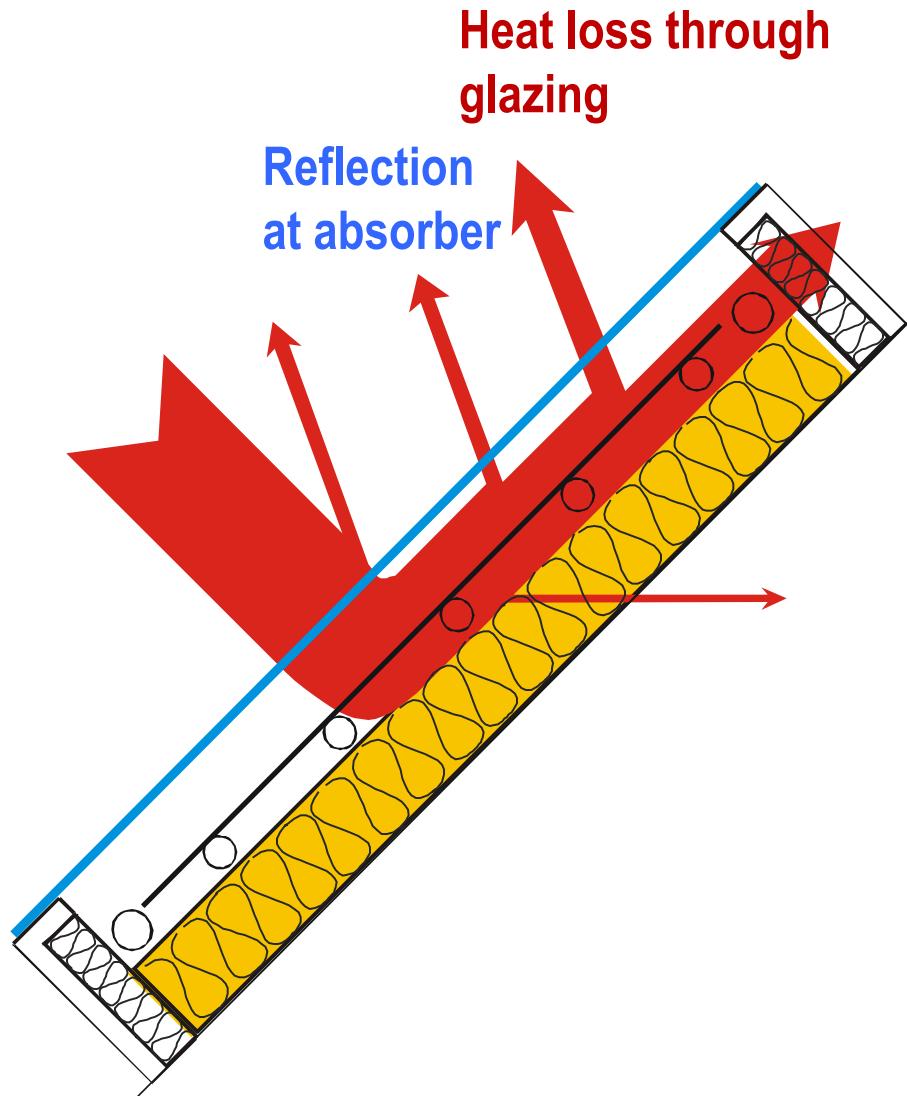
Antireflection (AR) coatings

reflection reduced to 1,5 % at each interface glass-iron
coating with low refraction index





Principle and balance of solar collector





Solar collector absorber

radiation properties for athermanous* bodies

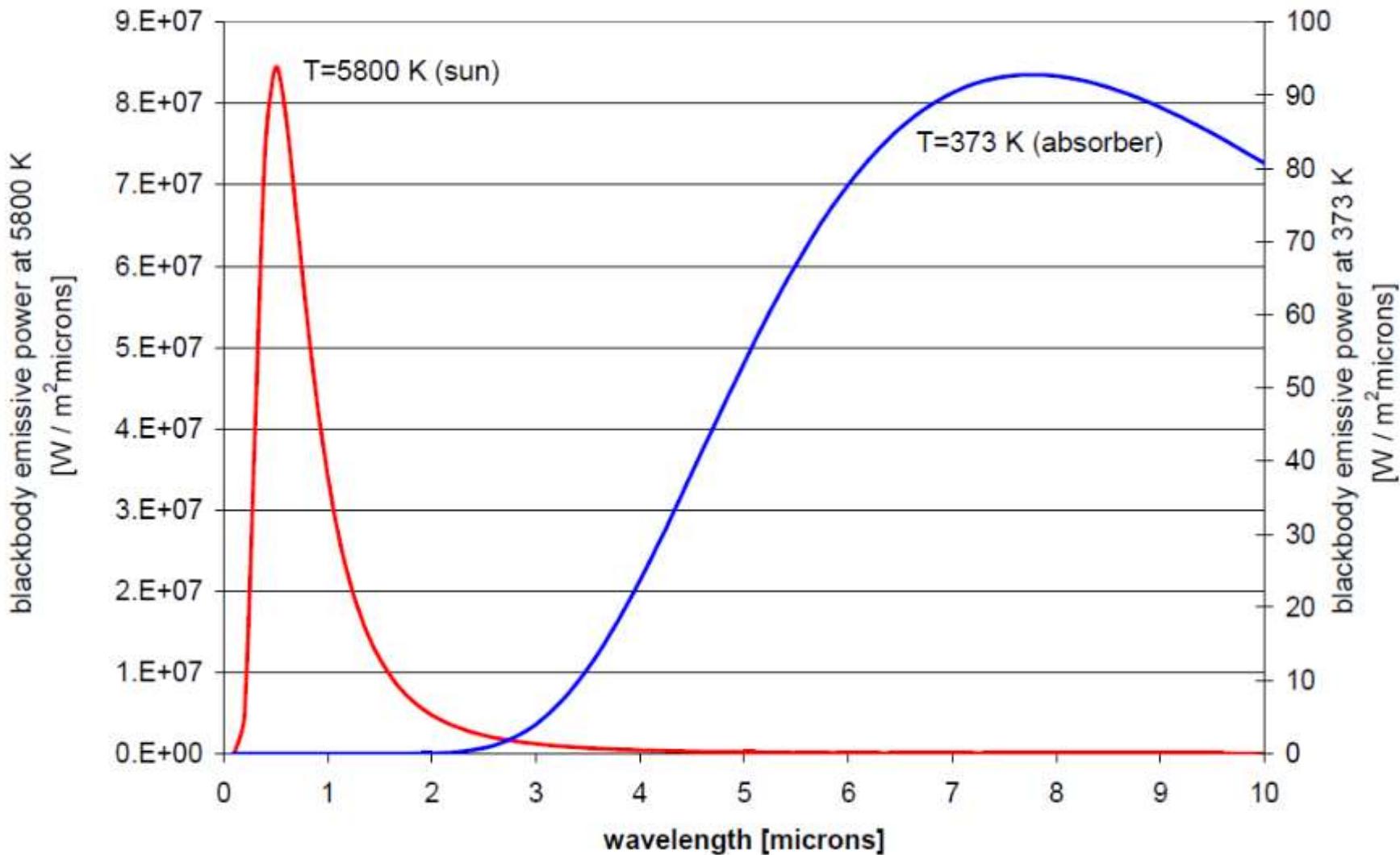
* Athermanous body is such a body through which any heat radiation cannot pass.

- absorptance α + reflectance $\rho = 1$
 - for given wavelength λ apply: absorptance α_λ = emittance ε_λ
-
- perfect black body: $\alpha = 1, \rho = 0$ for all wavelengths
 - perfect white body: $\alpha = 0, \rho = 1$ for all wavelengths
 - grey body $0 < \alpha = \alpha_\lambda < 1, \rho = 1 - \alpha$ for all wavelengths
 - **selective body** $0 < \alpha_\lambda < 1, \rho_\lambda = 1 - \alpha_\lambda$

$$\alpha_{\text{SOL}} \neq \varepsilon_{\text{IR}}$$

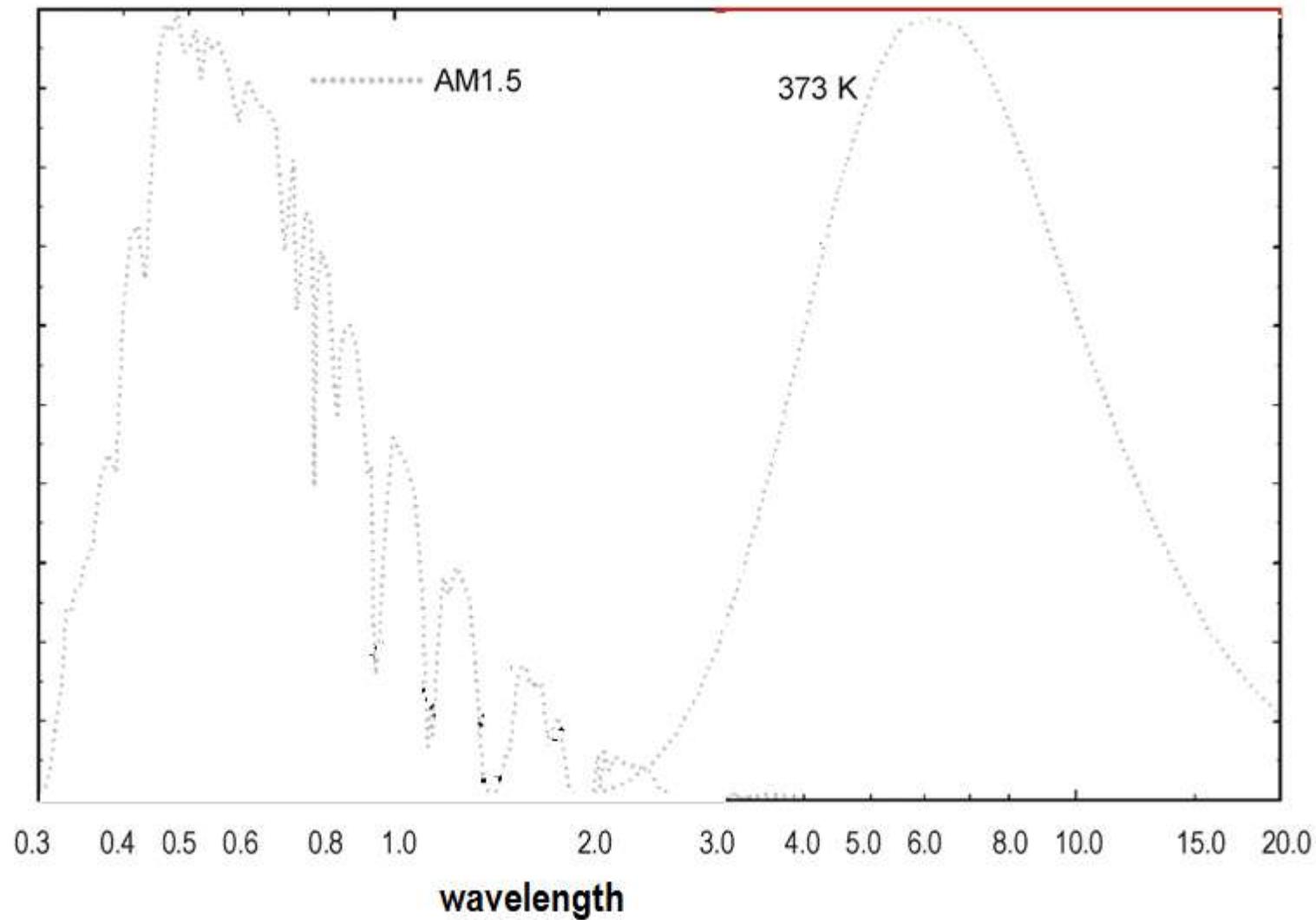


Black body emis. power 5800K ... 373K



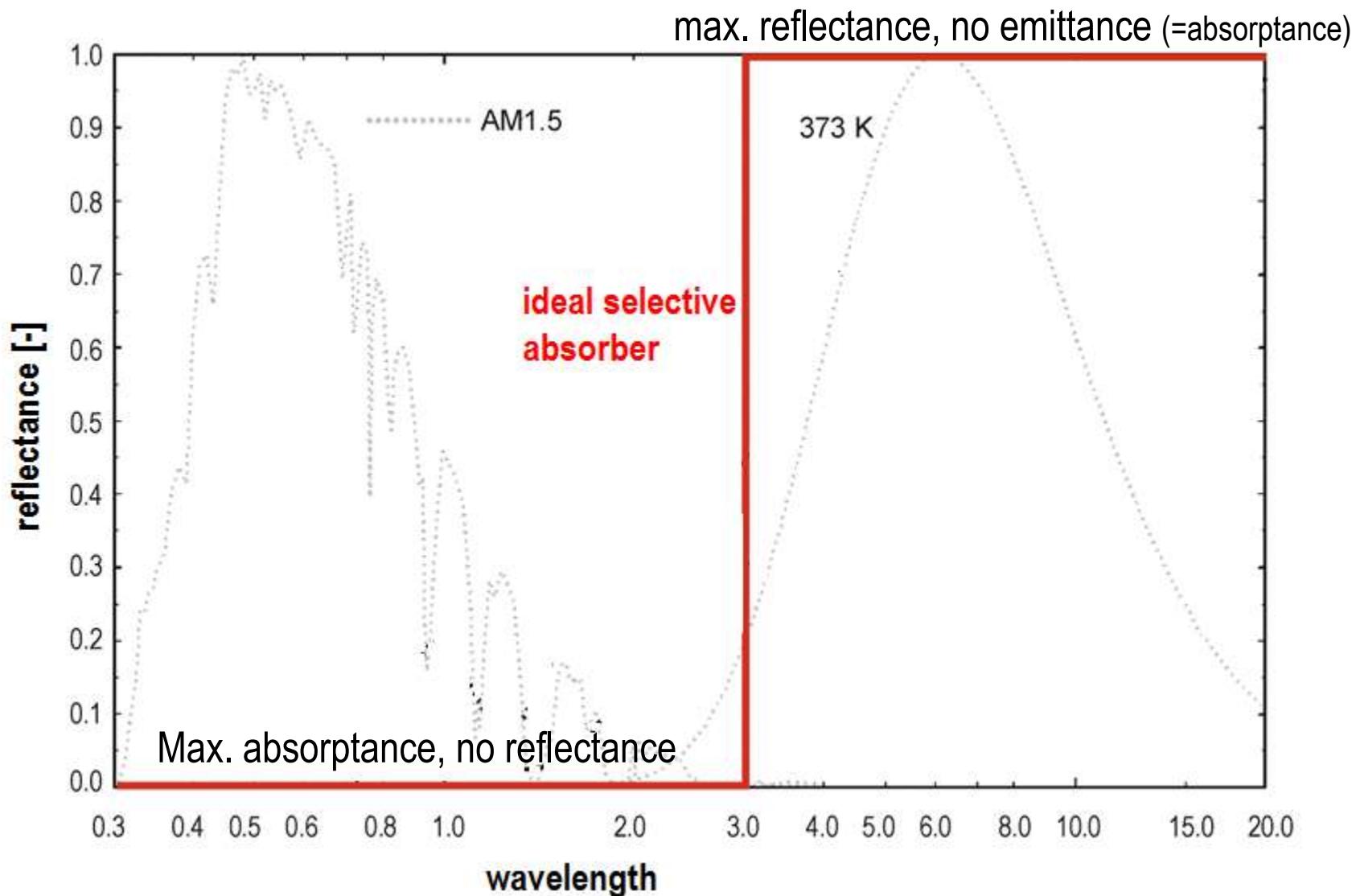


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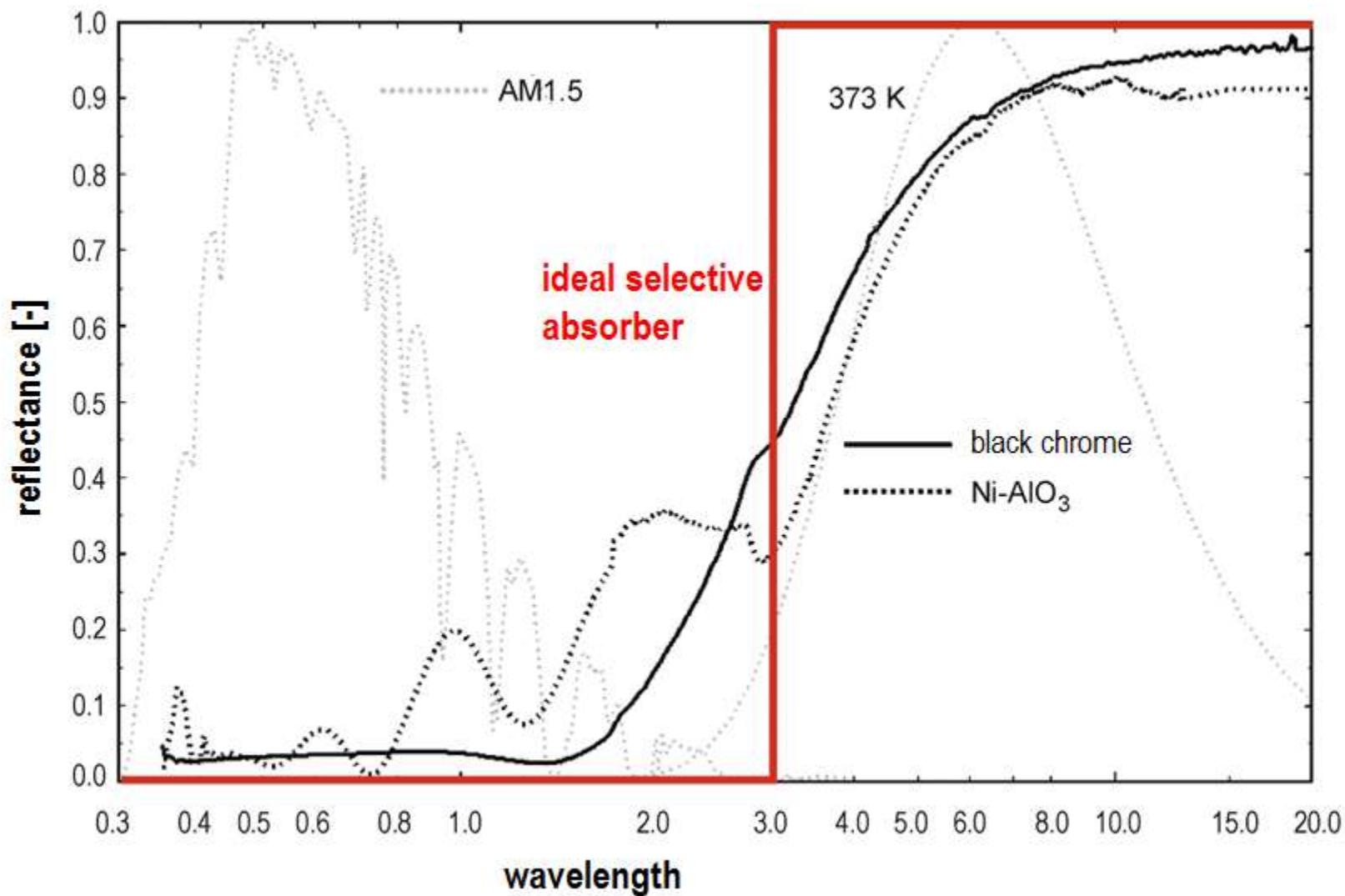


Absorber selectivity



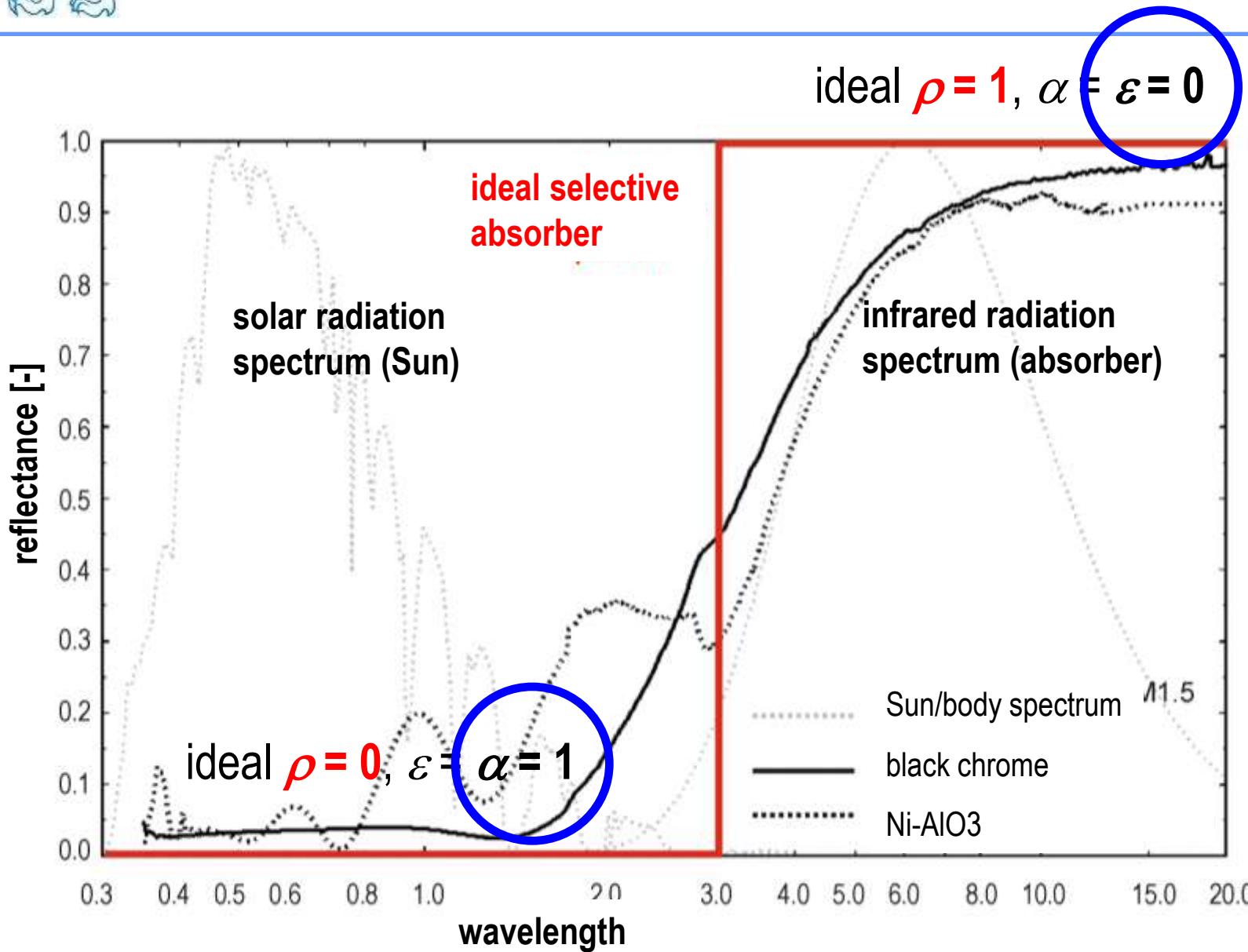


Absorber selectivity





Absorber selectivity





Selective surfaces

galvanic

- electrochemical process
- $\alpha = 0,93 - 0,96$, $\varepsilon = 0,10 - 0,16$

ceramic-metal (cermet)

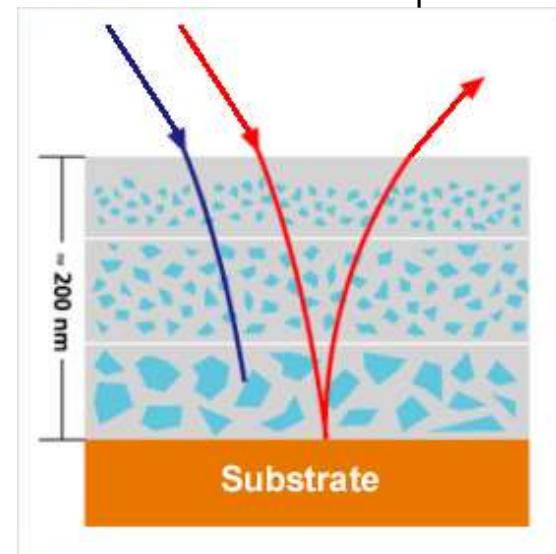
- sputtering, physical vapour deposition process, high quality surfaces
- $\alpha = 0,95$, $\varepsilon = 0,05$

paints

- considerably worse
- $\alpha = 0,92$, $\varepsilon = 0,85$

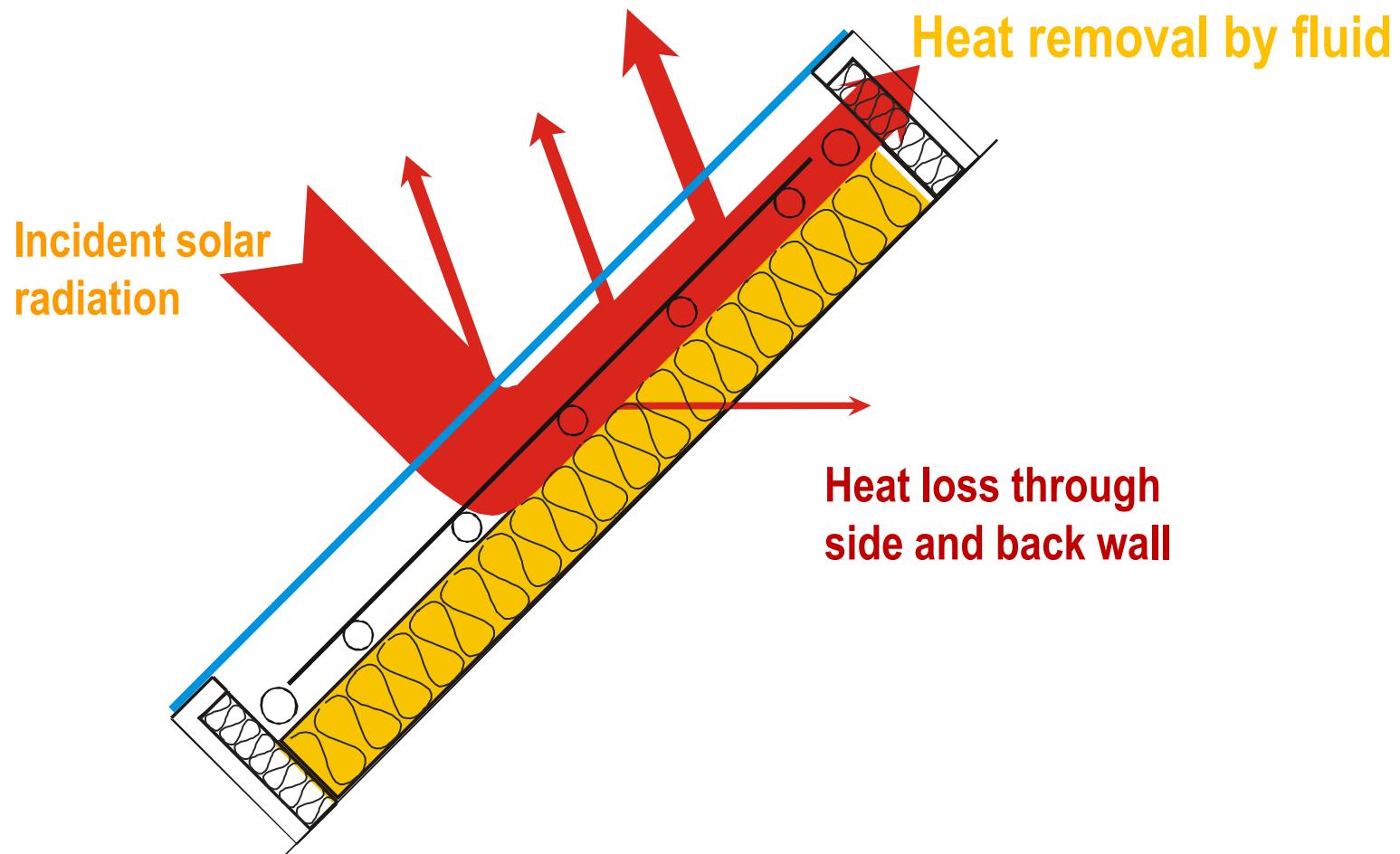


material goes from a condensed phase to a vapor phase and then back to a thin film condensed phase





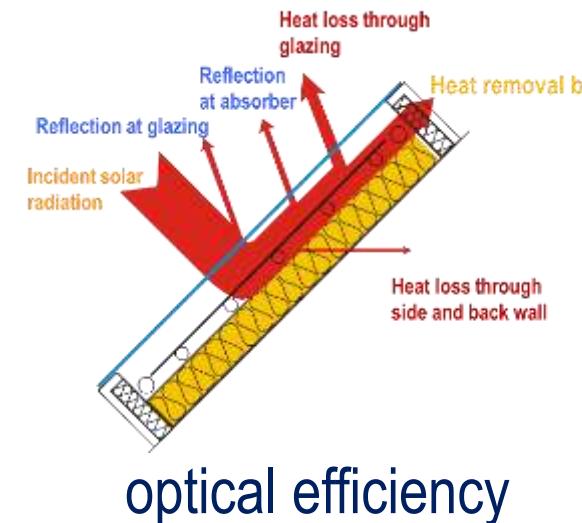
Principle and balance of solar collector





Efficiency of solar collector

$$\eta = \tau\alpha - U \frac{(t_{abs} - t_e)}{G}$$



τ ... glazing transmittance for solar radiation [-]

α ... absorber absorptance for solar radiation [-]

U ... heat loss coefficient [W/m².K]

t_{abs} ... mean absorber temperature [°C]

heat loss

t_e ... ambient temperature [°C]

G ... solar irradiance [W]



Simple calculation

collector	C1	C2
transmittance of collector glazing:	0,90	0,90
absorptance of collector absorber:	0,90	0,90
front U-value	6 W/m ² K	3 W/m ² K
back U-value	1 W/m ² K	1 W/m ² K

calculate efficiency for given conditions:

$$t_e = 10 \text{ } ^\circ\text{C}$$

$$G = 800 \text{ W/m}^2$$

$$t_{\text{abs}} = 20 \text{ } ^\circ\text{C} \qquad \qquad 80 \text{ } ^\circ\text{C}$$



Simple calculation

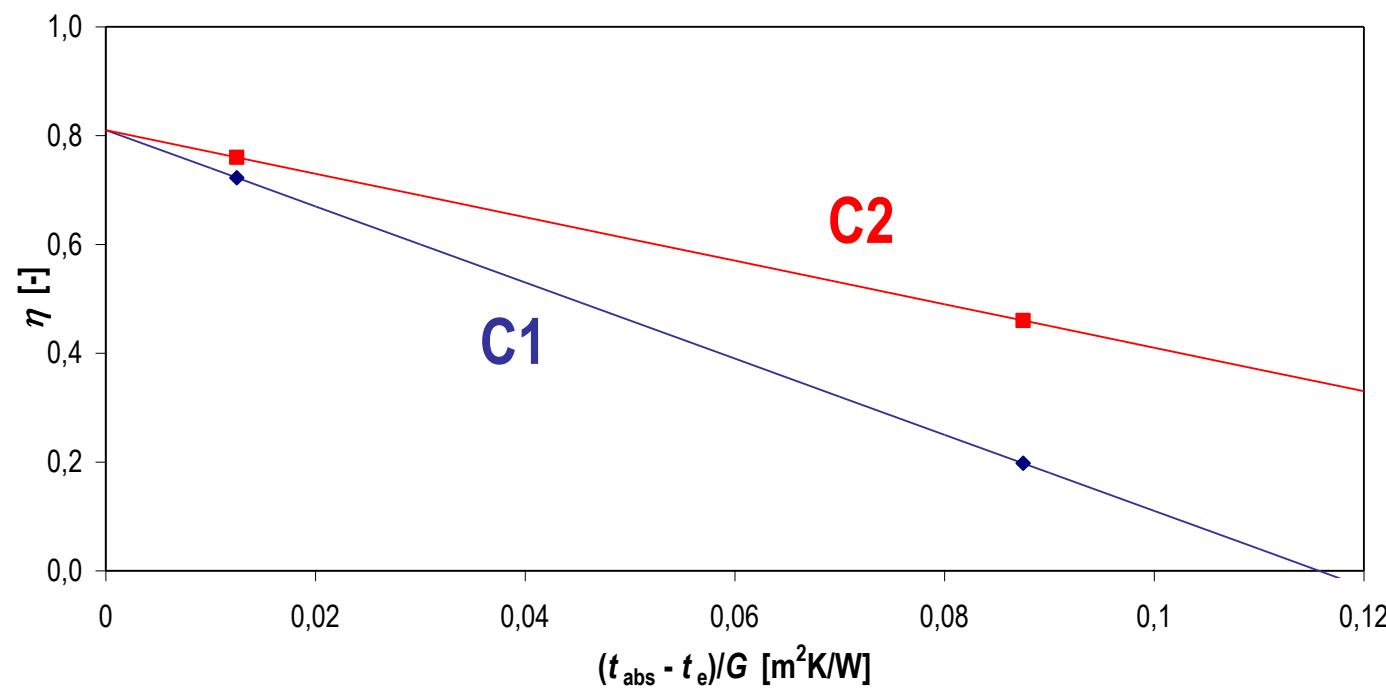
Collector 1

$$\eta = \tau\alpha - U \frac{(t_{abs} - t_e)}{G}$$

$$\eta = 0,9 \cdot 0,9 - (6+1) \frac{(t_{abs} - 10)}{800}$$

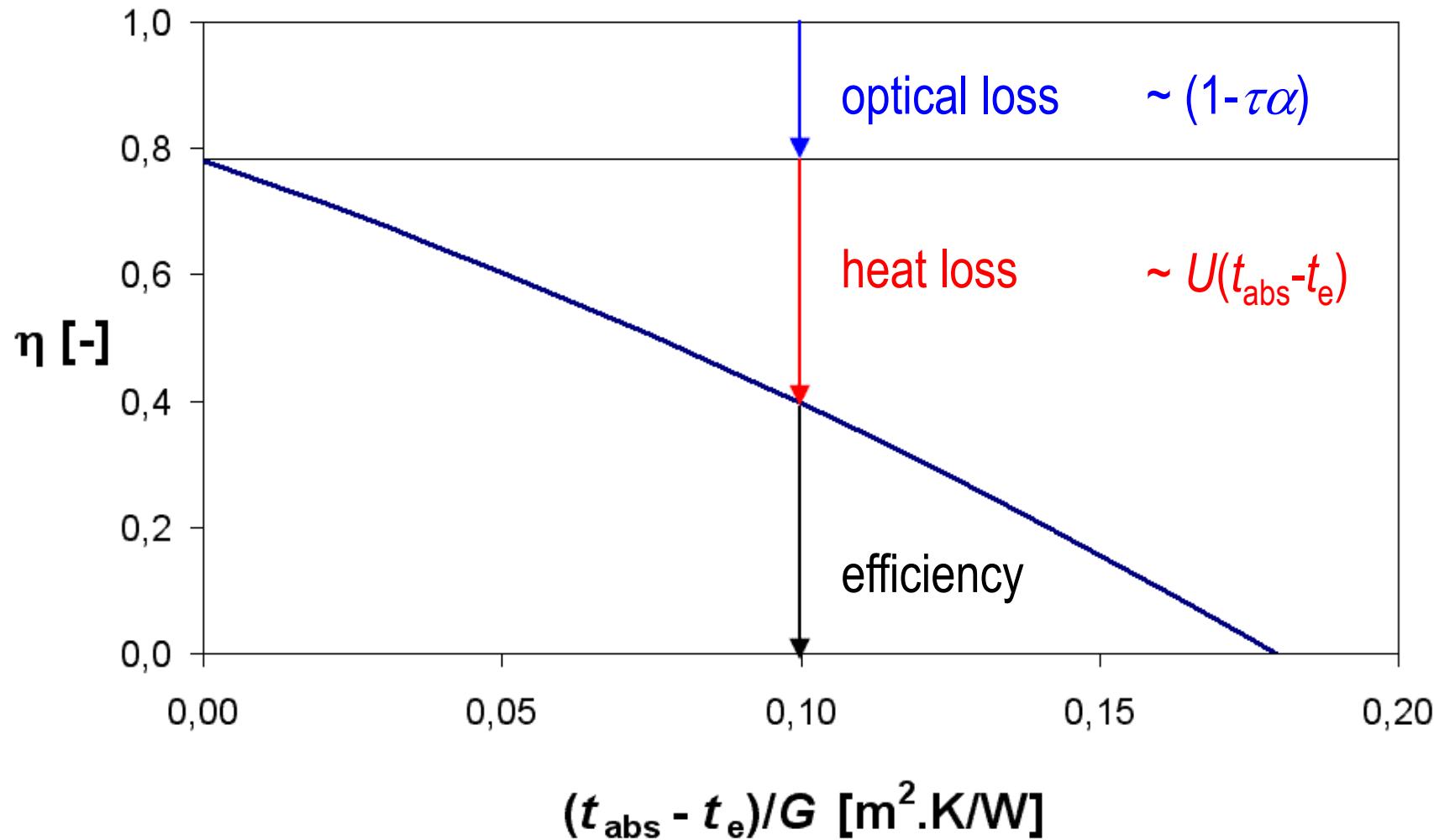
Collector 2

$$\eta = 0,9 \cdot 0,9 - (3+1) \frac{(t_{abs} - 10)}{800}$$





Efficiency of solar collector





Efficiency of solar collector

$$\eta = F' \cdot \left[\tau\alpha - U \frac{(t_m - t_e)}{G} \right]$$

F' ... efficiency factor > 0.90

depends on geometry and thermal properties of absorber

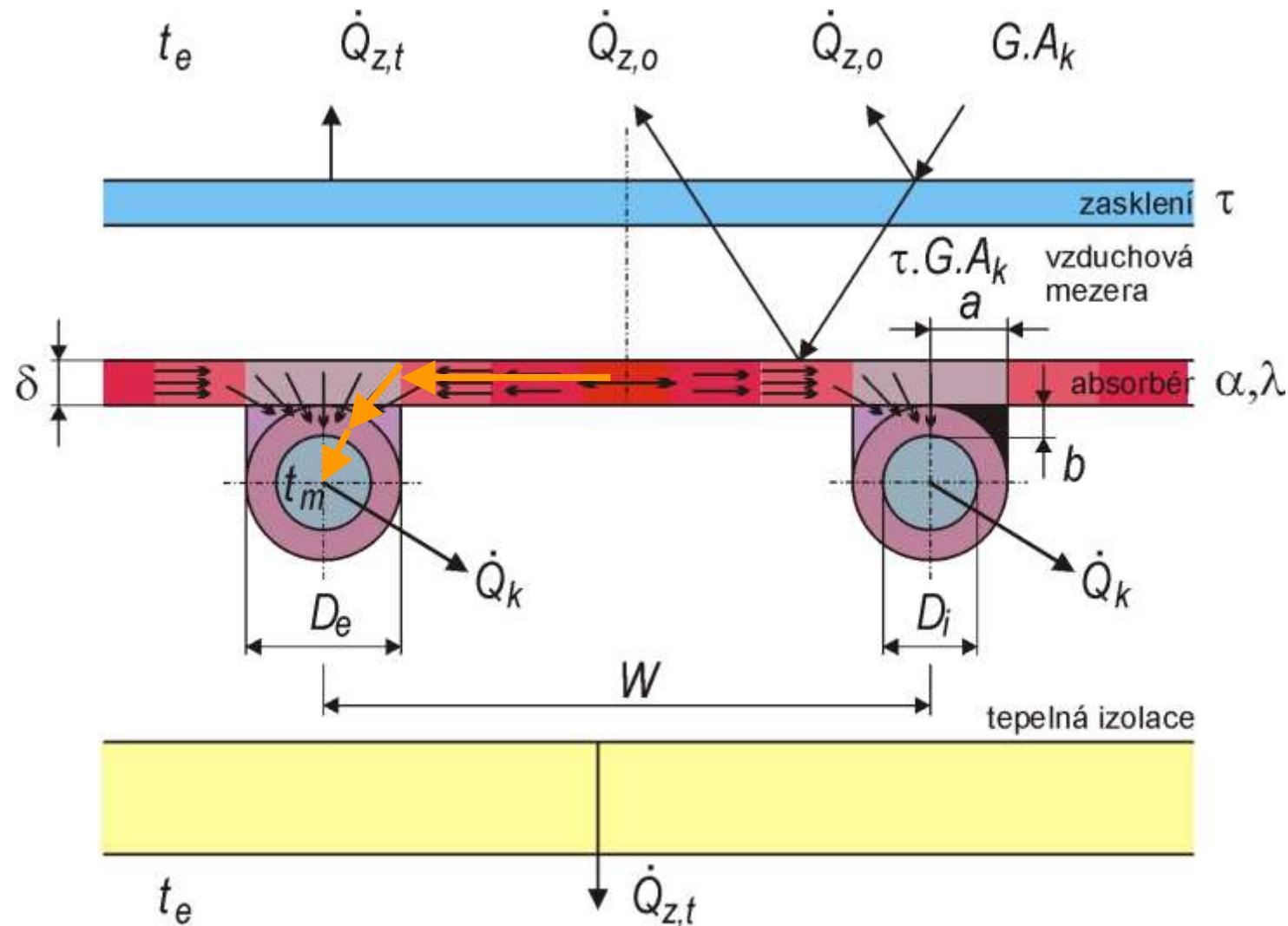
..... quality heat transfer from the absorber to the heat transfer fluid

t_m ... mean fluid temperature

$$t_m = (t_{k1} + t_{k2})/2$$



Heat transfer from absorber surface

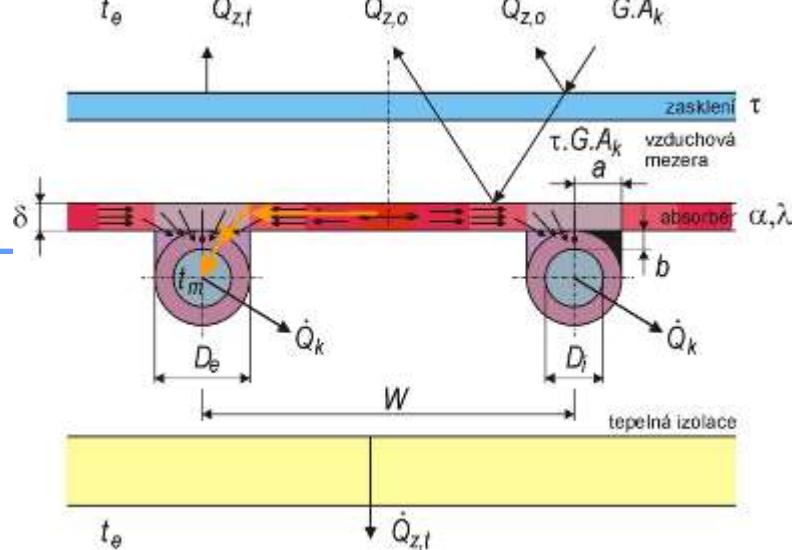




Efficiency factor F'

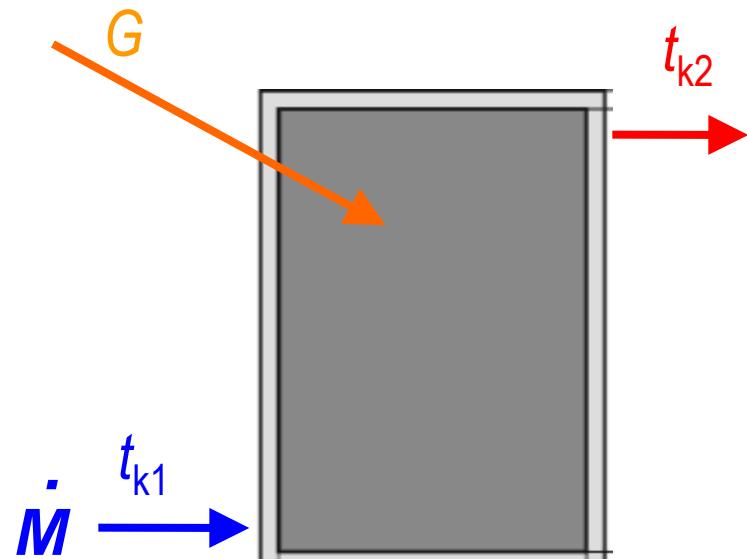
depends on

- geometry of absorber:
 - pipe distance, pipe dimension, thickness of pipe-absorber bond, absorber thickness
- physical properties of absorber:
 - thermal conductivity of absorber, thermal conductance of the bond pipe-absorber
- flow regime in pipes: **heat transfer from pipe wall to fluid**
- total heat loss coefficient of collector U





Determination of heat output by testing



heat output [W]

solar collector power

$$\dot{Q}_k = \dot{M} \cdot c \cdot (t_{k2} - t_{k1})$$

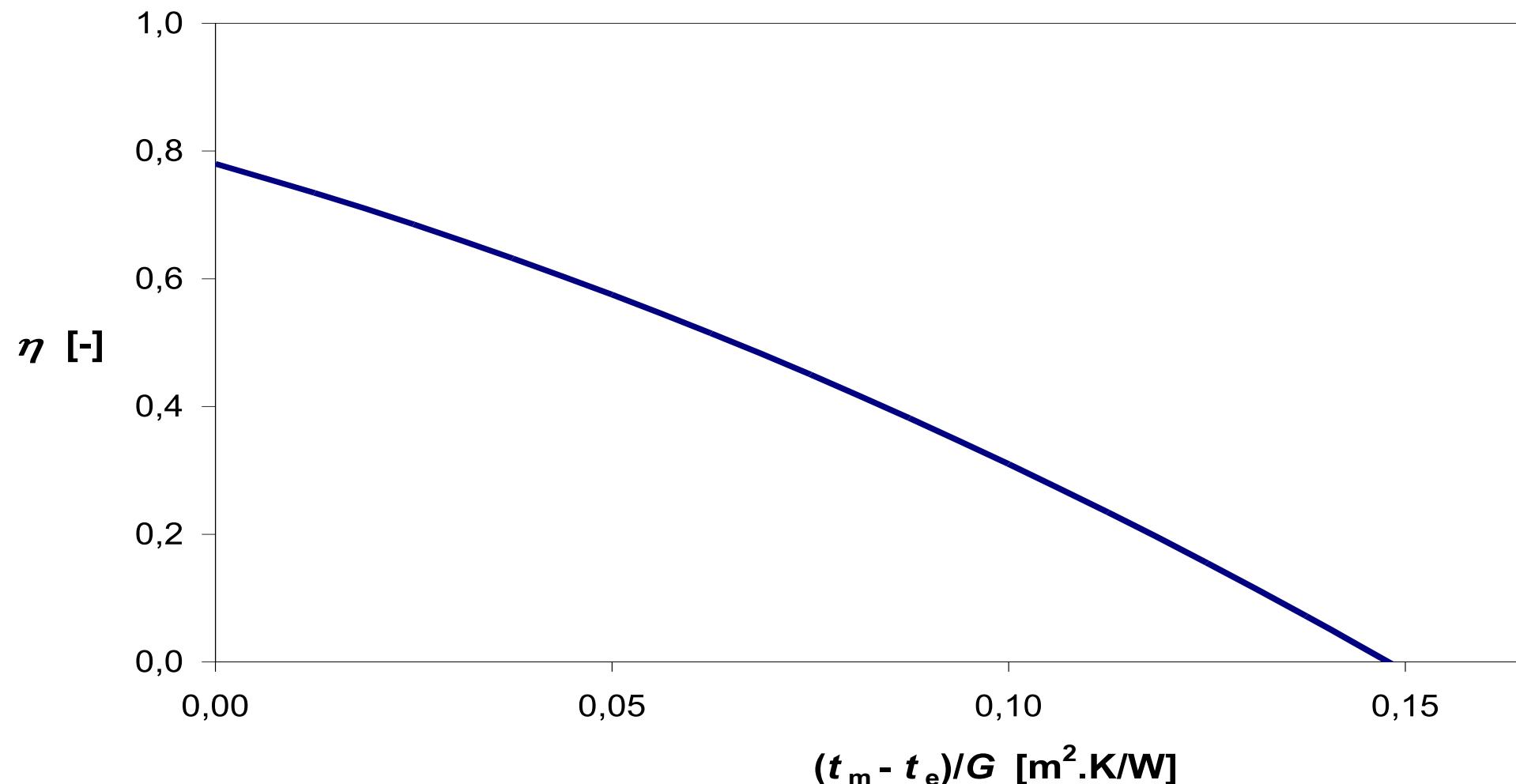
efficiency [-]

$$\eta = \frac{\dot{Q}_k}{G \cdot A_k}$$

tested at clear sky, $G > 700 \text{ W/m}^2$, normal incidence, $w > 3 \text{ m/s}$

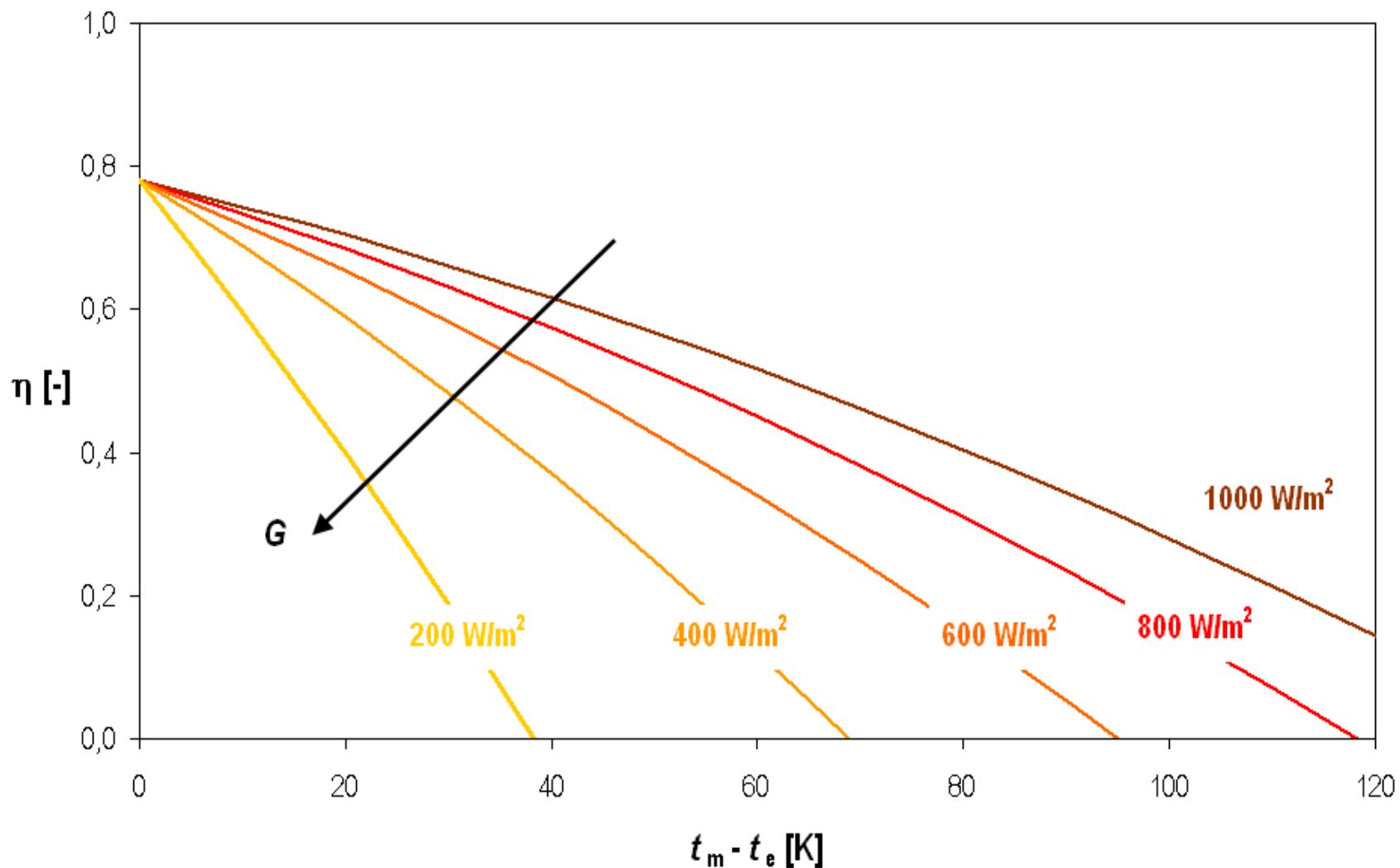


Efficiency characteristic



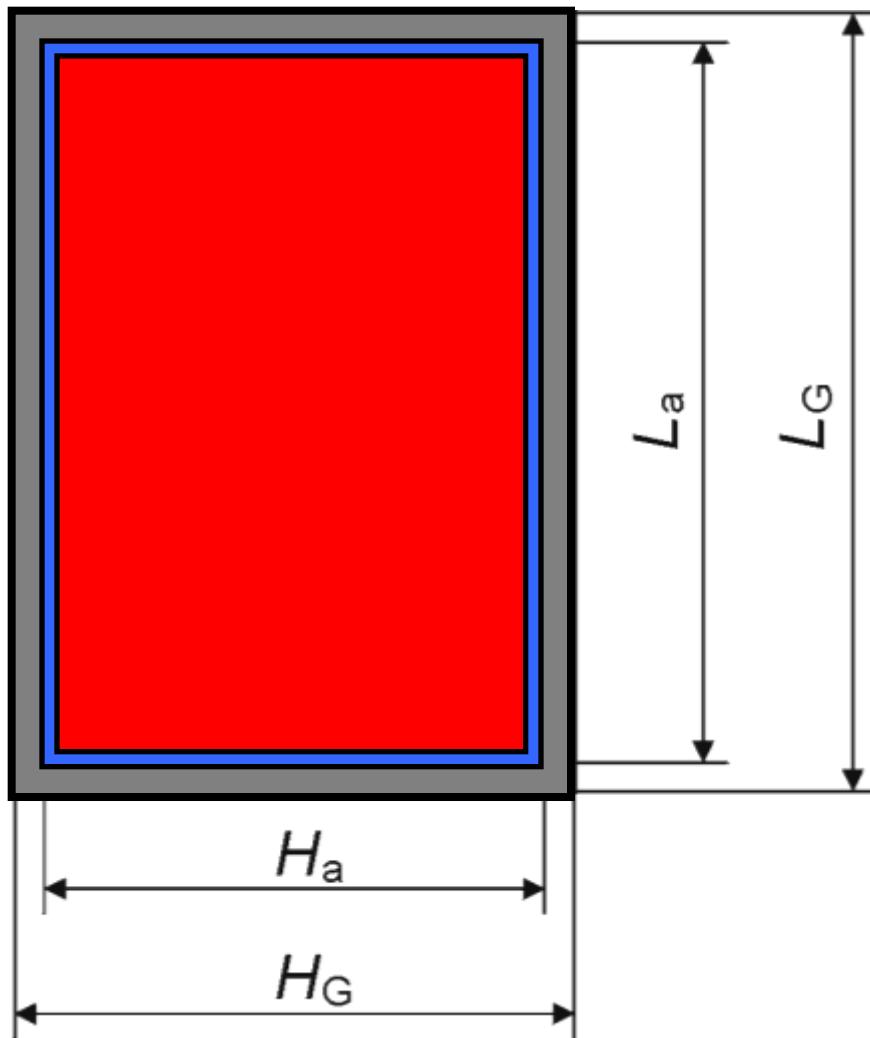


Efficiency characteristic = $f(t_m - t_e)$





Reference collector area A_k



$$\eta = \frac{\dot{Q}_k}{G \cdot A_k}$$

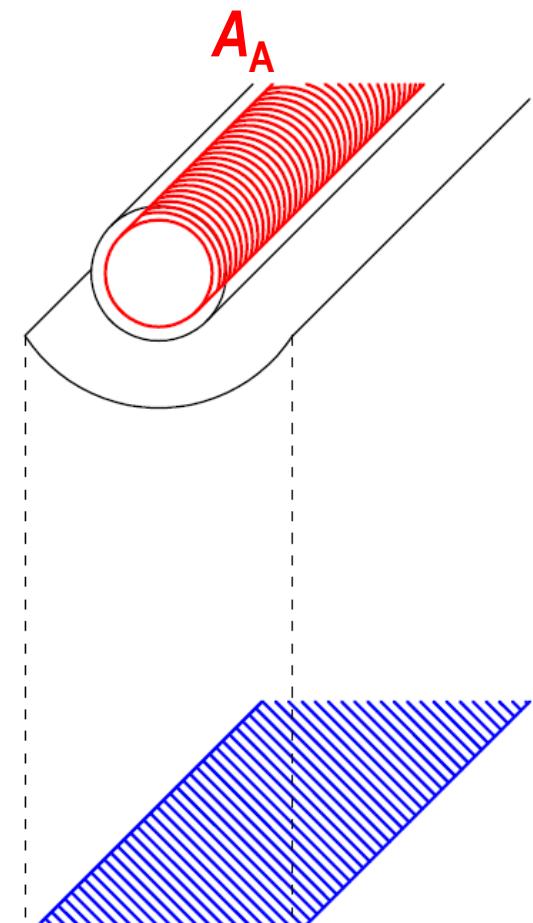
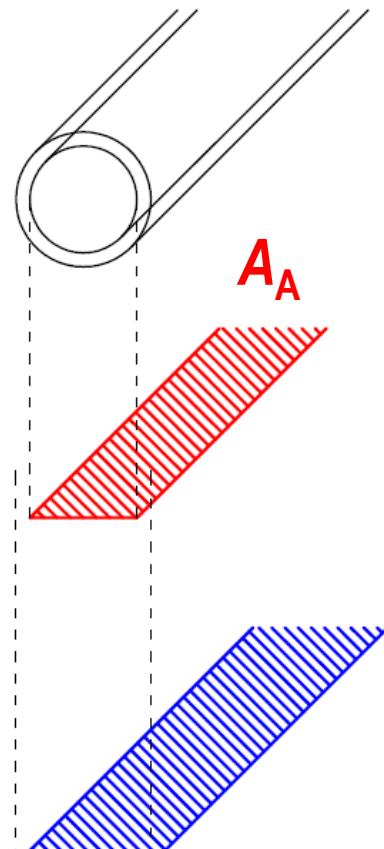
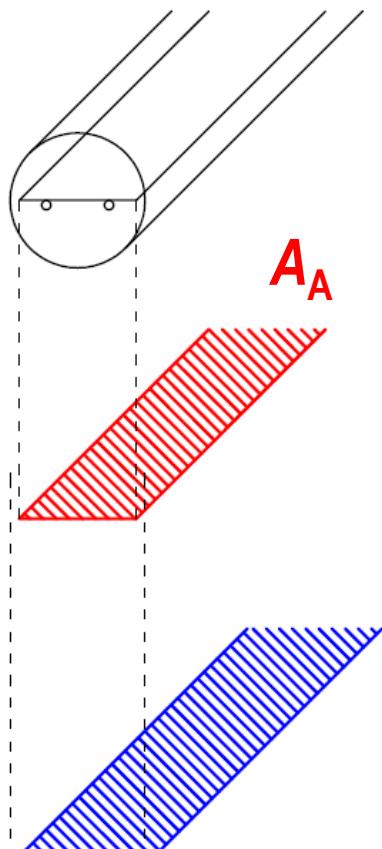
gross area: A_G

aperture area: A_a

absorber area: A_A

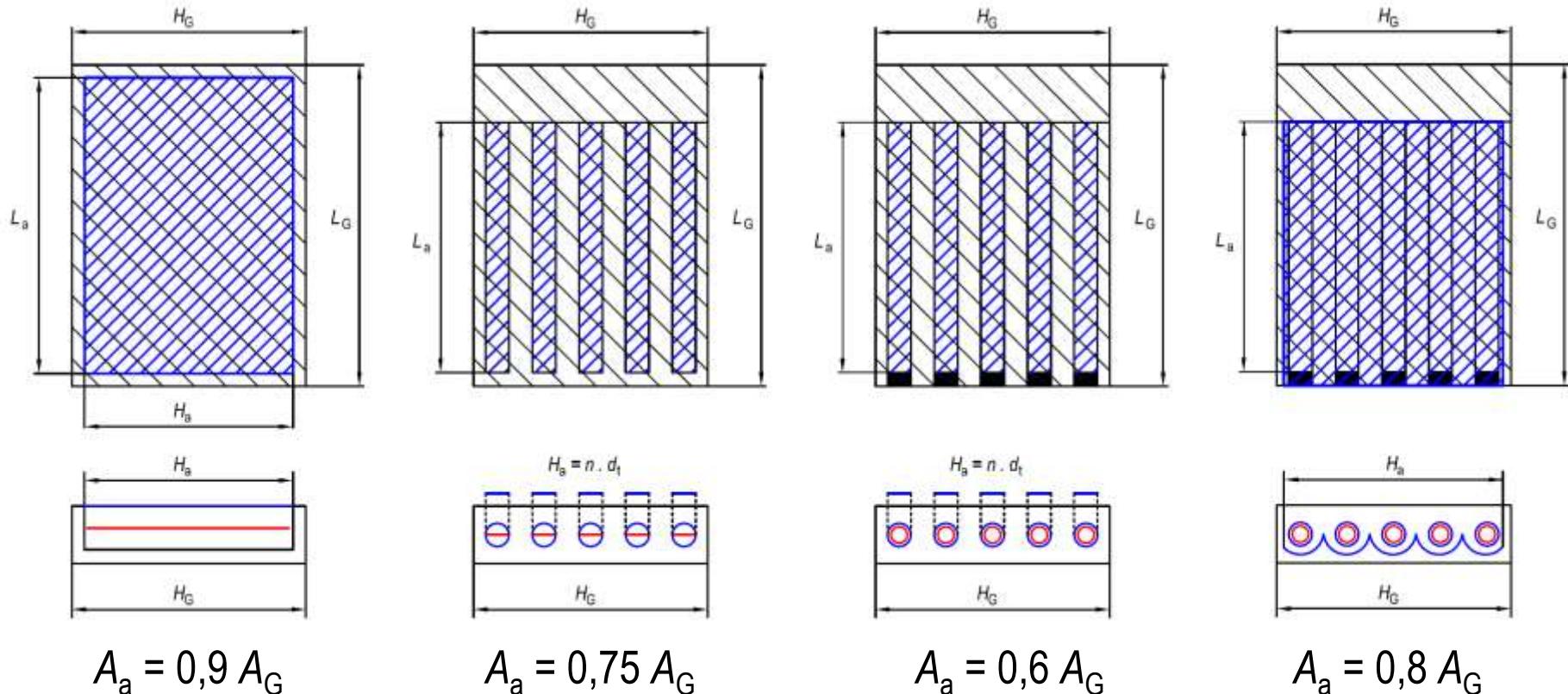


Reference collector area A_k





Reference collector area A_k



- aperture: comparison of collector quality, construction
- gross area: decision on potential for given application (limited space on roof)



Efficiency characteristic

$$\eta = \eta_0 - a_1 \cdot \frac{t_m - t_e}{G} - a_2 \cdot \frac{(t_m - t_e)^2}{G}$$

η_0 „optical“ efficiency [-], better: zero-loss efficiency

a_1 linear heat loss coefficient [W/(m².K)]

„related to difference between absorber and ambient temperature“

a_2 quadratic heat loss coefficient [W/(m².K²)] „simplified approach for the radiation losses“

values η_0 , a_1 , a_2 related to **reference area A_k (aperture is preferred)**

coefficients are given by producer, supplier or testing institute based on **test report in accordance to EN 12975-2**



Theory x testing

$$\eta = F' \tau \alpha - F' U \cdot \frac{t_m - t_e}{G}$$

$$\eta = \eta_0 - a_1 \cdot \frac{t_m - t_e}{G} - a_2 \cdot \frac{(t_m - t_e)^2}{G}$$

$\eta_0 = F' \tau \alpha$ *zero-loss efficiency*

$a_1 + a_2(t_m - t_e) = F' U$ *heat loss coefficient*



Typical coefficients *)

Collector type	η_0	a_1	a_2
	-	W/(m ² K)	W/(m ² K ²)
Unglazed	0.85	20	-
Glazed with nonselective absorber	0.75	6.5	0.030
Glazed with selective absorber	0.78	4.2	0.015
Vacuum single tube (flat absorber)	0.75	1.5	0.008
Vacuum tube Sydney	0.65	1.5	0.005

*) referenced to aperture area



Heat output (power) of solar collector

solar collector power (normal incidence, clear sky)

$$\dot{Q}_k = \eta \cdot A_k \cdot G = A_k [\eta_0 G - a_1 \cdot (t_m - t_e) - a_2 \cdot (t_m - t_e)^2]$$

η_0 „optical“ efficiency [-], a_1 linear heat loss c. [W/(m².K)] a_2 quadratic heat loss c. [W/(m².K²)]

installed (nominal) power

– for defined conditions (according to ESTIF):

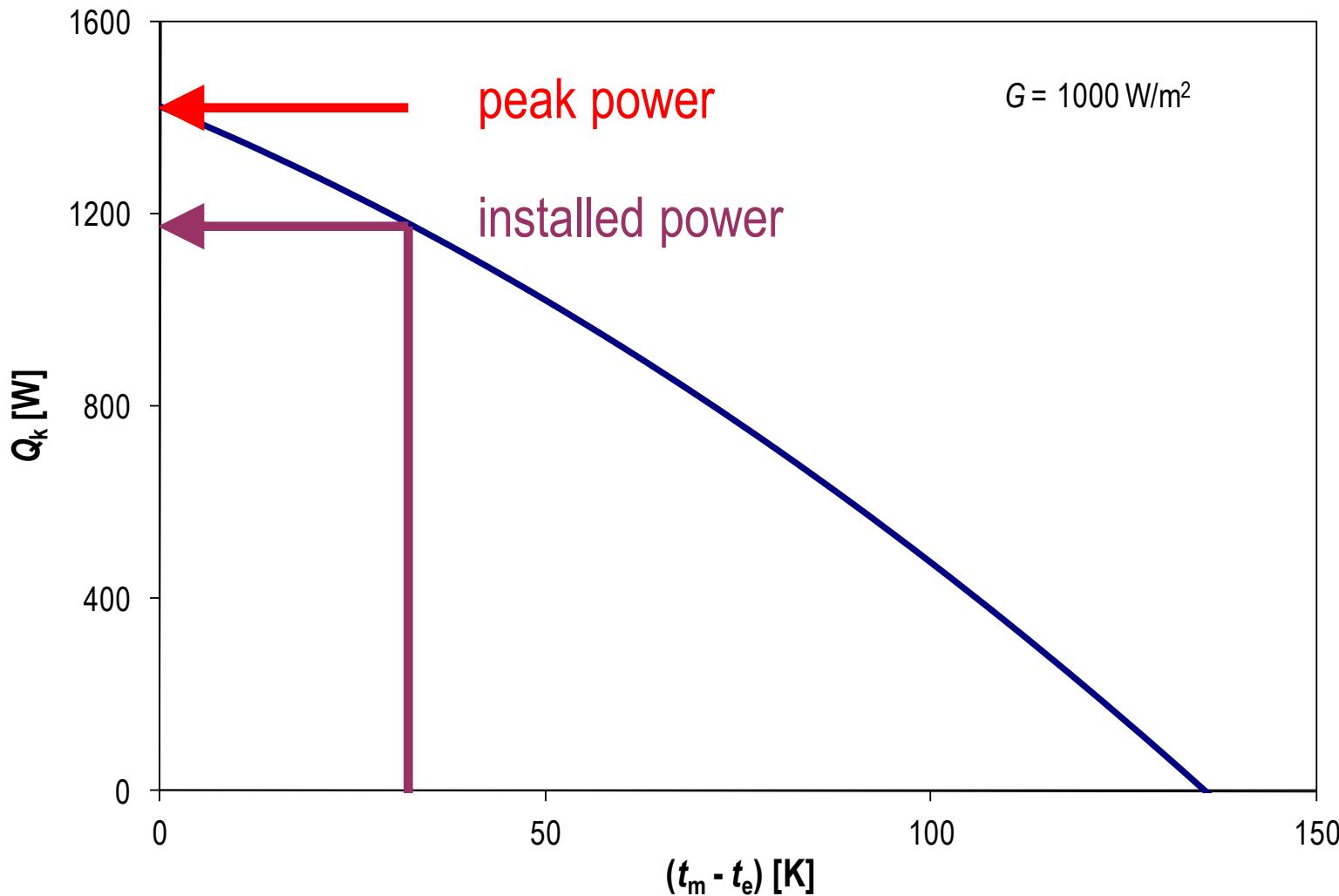
$$G = 1000 \text{ W/m}^2 \quad t_e = 20 \text{ }^\circ\text{C} \quad t_m = 50 \text{ }^\circ\text{C}$$

peak power (without heat loss)

$$\dot{Q}_{k,peak} = A_k \eta_0 G \quad G = 1000 \text{ W/m}^2$$



Heat output (power) of solar collector





Efficiency and power calculation

	flat-plate	vacuum tube	
$\eta_{0,a}$	0,75	0,65	-
$a_{1,a}$	3,5	1,5	W/m ² K
$a_{2,a}$	0,015	0,005	W/m ² K ²
A_G	4		m ²
A_a	3,6	2,4	m ²

**calculation of daily efficiency for April,
Prague city, slope 45°, azimuth 45°**

$G_{T,m}$	473	W/m ²
$t_{e,s}$	12,1	°C
$t_{k,m}$	40	°C



Efficiency and power calculation

$$\eta_k = \eta_0 - a_1 \cdot \frac{t_{k,m} - t_{e,s}}{G_{T,m}} - a_2 \cdot \frac{(t_{k,m} - t_{e,s})^2}{G_{T,m}}$$

$$\dot{Q}_{k,m} = \eta_k \cdot A_k \cdot G_{T,m}$$

$$Q_{k,day} = \eta_k \cdot A_k \cdot H_{T,day}$$

- mean daily solar irradiance

$$G_{T,m} = \frac{H_{T,day,th}}{\tau_t}$$

- daily solar irradiation
- $$H_{T,day} = \tau_r \cdot H_{T,day,th} + (1 - \tau_r) \cdot H_{T,day,dif}$$

$$H_{T,day} = 3.64 \text{ kWh/m}^2\text{.day}$$

	flat-plate	vacuum tube	
η_k	0,52	0,55	-
$Q_{k,m}$	884	628	W
$Q_{k,day}$	6,8	4,8	kWh/day



Nominal conditions (ESTIF)

$$\dot{Q}_{k,peak} = A_k \eta_0 G$$

	flat-plate	vacuum tube	
G	1000		W/m ²
$t_{e,s}$	20		°C
t_m	50		°C
η_k	0,63	0,60	
$Q_{k,nom}$	2273	1441	W
$Q_{k,peak}$	2700	1560	W



Solar collector / applications

